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Small Caliber Cartridge Case Annealing brass for grain configuration **SCAMP**

20. ABSTRACY (Continue on severae side if necessary and identify by block number)

This report describes a proposed 3-draw process utilizing the standard U.S. cup on a modified Small Caliber Ammunition Modernization Program (SCAMP) Case Submodule at Lake City AAP to manufacture 7.62mm cartridge cases that would satisfy the U.S. NATO grain configuration requirements.

TABLE OF CONTENTS

SEC	TION . PAI	3E
1.	SUMMARY	1
2.	INTRODUCTION	2
3.	OBJECTIVE	3
4.	PLAN	4
5.	PROPOSED PROCESS	6
6.	TOOLING DEVELOPMENT	8
	6.1 Equipment	8
	6.2 Effect of Tool Modifications	8
	6.3 Final Tool Designs	2
7.	ANNEALING DEVELOPMENT	3
	7.1 Equipment	3
	7.2 Coil Design	9
	7.3 Final Configuration	C
	7.4 Void Tests	2
8.	IN-PROCESS PART DEFINITIONS	5,
9.	FINISHED PART INSPECTION	7
	9.1 Dimensional	7
	9.2 Metallurgical	7
10.	TEST FIRING	8
11.	SCAMP EQUIPMENT CHANGES	9
	11.1 Tooling	9
	11.2 Basic Equipment	9
	11.3 Layout 3	1
12.	CONCLUSIONS	4
	ILLUSTRATIONS	
FIG	URE NO. PAG	36
1.	DEVELOPMENT HISTORY	5
2.	PROPOSED PROCESS	7
3.	TAPER TOOL MODULE	9.
4.	TAPER SIMULATOR AND TOOL MODULE	0

TABLE OF CONTENTS

(Continued)

URE NO.	AGE
INDUCTION TEST RIG SCHEMATIC	14
INDUCTION TEST RIG	15
QUENCH AND BLOW OFF CHAMBER	16
BODY ANNEAL INDUCTION COIL	25
DRAW PUNCH SLEEVE	30
EQUIPMENT LAYOUT SCHEMATIC	32
ATTACHMENTS	
ACHMENT NO.	
TOOL DRAWINGS .	
COIL DRAWINGS	
IN-PROCESS PART DEFINITIONS	
DIMENSIONAL INSPECTION DATA	
METALLURGICAL INSPECTION DATA	
TEST FIRING DATA	
-	INDUCTION TEST RIG SCHEMATIC INDUCTION TEST RIG QUENCH AND BLOW OFF CHAMBER BODY ANNEAL INDUCTION COIL DRAW PUNCH SLEEVE EQUIPMENT LAYOUT SCHEMATIC ATTACHMENTS ACHMENT NO. TOOL DRAWINGS COIL DRAWINGS IN-PROCESS PART DEFINITIONS DIMENSIONAL INSPECTION DATA METALLURGICAL INSPECTION DATA

1. SUMMARY

This document reports the activities and results of a program carried out by the Advanced Development and Engineering Center of GULF + WESTERN to develop a process to manufacture 7.62 mm cartridge cases on SCAMP equipment. The program was funded by ARRADCOM under Contract Number DAAK10-78-C-0165, which followed G+W Proposal Number 15506A.

The program plan was based on a tentative process mutually arrived at by ARRADCOM and G+W in which the critical tasks were: (a) developing a three-draw process from the specified standard U.S. cup using one inter-draw anneal; and, (b) developing an induction anneal system to satisfy the U.S. - N.A.T.O. grain specifications.

All development work was carried out at the G+W Folcroft facility using G+W press simulators and a specially designed induction anneal test rig. Although this equipment is manually operated, the various operations of the SCAMP equipment are closely simulated in terms of metalforming and heating functions.

The program was successful in accomplishing its objectives and culminated in the supply of a small quantity of cartridge cases to ARRADCOM for evaluation and test firing.

2. INTRODUCTION

Over the last decade, G+W has been responsible for the conception and development of high speed rotary ammunition systems as part of an extensive modernization program carried out under the auspices of the P.B.M. office of ARRADCOM.

The systems are now installed at L.C.A.A.P. and are producing 5.56 mm caliber ammunition. The systems were designed to be compatible with conversion to produce other caliber sizes. However, it was also recognized that some addition to, or modification of, the basic equipment may be necessary to accommodate differences in processes appropriate to other calibers.

G+W has supplied systems to overseas customers which produce 7.62 mm as well as 5.56 mm ammunition and, in doing so, has developed suitable processes. However, the U.S. - N.A.T.O. requirements define a specific grain structure and ARRADCOM also stipulated that the standard U.S. cup must be used. These factors introduced complications of process beyond those already developed.

G+W Proposal Number 15506 resulted in ARRADCOM placing a contract to develop a process which would fulfill the requirements and be compatible with SCAMP equipment.



Advanced Development and Engineering Center

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3. OBJECTIVE

The objective of the program was to establish a process to produce 7.62 mm, M80 cartridge cases on a SCAMP sub-module at 1200 parts per minute.

Program completion would be recognized with submission of: (a) 1,000 acceptable 7.62 mm cases to Drawing Number 10521997 with applicable grain specification and, (b) a final technical report.

A contract modification added a test to evaluate the effect of voids (missing parts) in the transport chain on the performance of the anneal system.

4. PROGRAM PLAN

The plan which was prepared and generally followed is outlined below:

- 1. Identify differences between the proposed 7.62 mm process and the current 5.56 mm SCAMP process, then develop the proposed process and define the methods of showing compliance with the product specification.
- Design and procure the necessary developmental tooling and equipment, including an induction anneal system.
- 3. Set up simulators, tool modules, induction anneal system and processing equipment.
- 4. Develop tooling and induction anneal process to obtain required dimensional and metallurgical properties.
- 5. Perform measurements of in-process dimensions, head hardness, hardness gradient and grain structure to define in-process part characteristics.
- 6. Produce a small batch of finished parts for Government evaluation and process approval.
- 7. Produce 1,000 parts to be test-fired by the Government.
- 8. Develop final recommended process flow diagrams and in-process part specifications.
- 9. Prepare a final technical report.
- 10. Deliver items as follows:
 - (i) Progress reports
 - (ii) Final technical report
 - (iii) 1,000 finished cases
 - (iv) Tools and test equipment procured under the contract

The only significant deviation occurred in relation to Item 6, above, in that three series of samples were produced and evaluated before approval to proceed was granted.

Test series A produced parts with dimensional discrepancies. Test series B resulted in minor dimensional discrepancies and ARRADCOM requested a further series C which would use L.C.A.A.P. process specifications where appropriate, as well as correcting the deviations.

The actual timetable of activities is summarized in Figure 1.

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Figure 1 PROGRAM HISTORY

5. PROPOSED PROCESS

Referring to Figure 2, the ARRADCOM stipulation was that the process should use the standard U.S. cup, Drawing Number 10522459. It was considered that the geometry of this cup, with consequent high area reduction through the final draw, mandated a three-draw process.

The second consideration was that, in order to attain the specified grain structure, an anneal would have to be performed between second draw and final draw.

The third consideration was the addition of a pre-pocket operation prior to heading so as to have a reliable primer pocket condition and adequate internal head hardness.

The remainder of the process is similar to the 5.56 mm SCAMP process.

By comparison, the conventional 7.62 mm process has an additional anneal between first draw and second draw, a machine trim instead of pinch trim and additional wash, lube and dry operations.

CUP FIRST' DRAW SECOND DRAW WASH, ANNEAL, QUENCH, PICKLE, RINSE/LUBE THIRD DRAW/PINCH TRIM POCKET HEAD HEAD' TURN PIERCE WASH, BODY ANNEAL, QUENCH, LUBE FIRST TAPER SECOND TAPER, PLUG FINAL TRIM WASH, STRESS RELIEF ANNEAL PICKLE, RINSE NECK & MOUTH ANNEAL

FIGURE 2 PROPOSED PROCESS

FINISHED CASE

6. TOOLING DEVELOPMENT

Following the process selection described in Section 5, tentative in-process part specifications were generated. Using these as a basis, tooling was designed and fabricated to accomplish all operations. The development program began with these designs which were modified as the program progressed.

The development was an iterative process involving minor changes of tooling design and in-process part specifications to achieve the desired final case characteristics. Some of the detail effects of tool design changes will be briefly discussed.

6.1 Equipment

All development work was carried out using SCAMP tool modules and simulators.

A tool module is an assembly which contains all the tools necessary to perform a particular metal-working operation. By virtue of the design, tool adjustment is precisely controlled within the module and the whole assembly can be quickly installed in the SCAMP rotary presses. It can also be installed and used in a simulator, which is a single-station machine designed to duplicate the essential features (displacement, for example) of a rotary press.

The original reason for the tool module/simulator concept was to facilitate off-line tool check-out but it is also eminently suitable for tooling and process development, as in this program.

Experience has shown that there is good correlation between simulator and rotary press process performance so that the results of this program can be expected to be valid in predicting the effects of sub-module conversion.

A typical tool module is shown in Figure 3, and is shown installed in the appropriate simulator in Figure 4..

6.2 Effect of Tool Modifications

Changes were made to tool designs in three areas, affecting draw die angles, second draw punch profile and pre-pocket nib configuration.

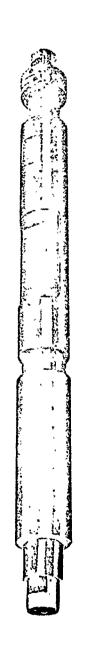


FIGURE 3 TAPER TOOL MODULE

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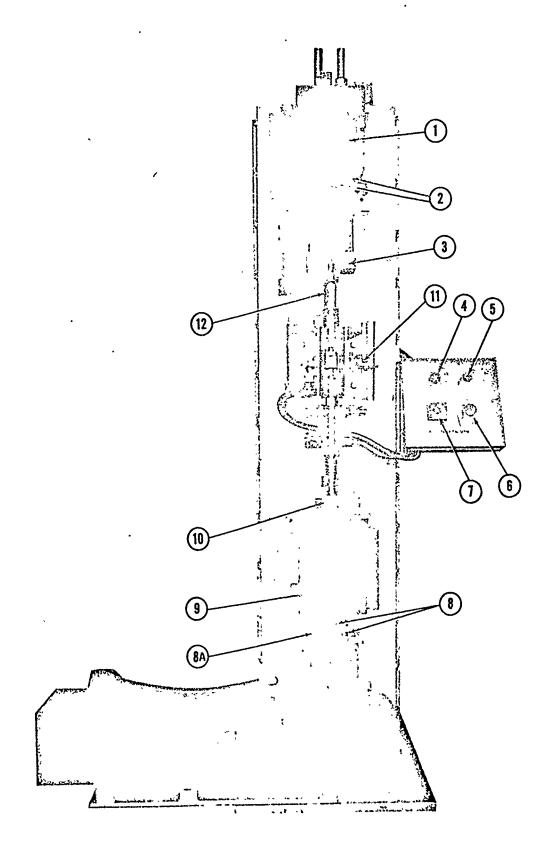


FIGURE 4 TAPER SIMULATOR AND TOOL MODULE

6.2.1 Draw Die Angles

During test series A, various combinations of draw die angles were tried to achieve what was judged to be a desirable base thickness (and consequently web thickness). The resultant selection was also used for test Series B. However, the incorporation of the L.C.A.A.P. process guide in the scope of work prior to Series C, necessitated further changes (reduction of die entry angles) to achieve the increased base (and web) thickness.

6.2.2 Second Draw Punch

The surface hardness measurements of series A and B showed a dip at the 0.75 inch point which could not be eliminated by adjustments of the body anneal coil. Although the resulting hardness profile was within the prescribed limits, it was decided that a better safety margin would exist if the dip could be alleviated.

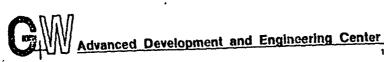
The approach taken was to study the second draw and final draw tooling to establish the degree of metal-working occurring from the second draw part to the final draw part at several axial locations. This revealed that the metal at the 0.75 inch point had undergone less working than adjacent points and, in fact, did not fit a smooth curve drawn through all points.

Accordingly, the second draw punch profile was slightly modified and was successful in producing the desired result.

6.2.3 Pre Pocket Nib

Two nib configurations were tried initially, one having a straight taper profile and one having a hemispherical profile. The former was selected on the basis of its attaining a slightly greater head hardness. At the conclusion of test series B, ARRADCOM engineers detected an imperfection of the final pocket in the form of a small groove about half-way down the pocket and extending for about one-quarter of the circumference. Ammunition manufacturing terminology refers to this condition as a "rill", and is thought to cause primer leaks.

It was found that the alternate configuration did not produce the defect and it was used for the remainder of the program.



6.3 Final Tool Designs

1.7

A list of drawings of the final recommended tool designs and a reduced copy of each is included as Attachment 1. The original tracings were supplied to ARRADCOM.

7. ANNEALING DEVELOPMENT

7.1 Equipment

To properly conduct all the various annealing tests that had to be performed, a test rig was designed and constructed, see Figures 5, and 6 This facility has all the necessary instrumentation required to monitor and control all known annealing process parameters. Power, chain speed, water temperature and pressure, time until quench, and coil dimensions are all adjustable to allow a thorough evaluation of the pertinent variables so that the process could be optimized. A brief description of each of the components in the system is given below:

7.1.1 Inverter

The inverter is a 200 kw, 10 kHz solid state unit with digital power monitor. It converts the 460 volt, 60 Hz, 3 phase electrical input into 440 volt, 10 kHz, single phase output, which is connected to the heat station.

7.1.2 Heat Station

The heat station is used to obtain an oscillating, or resonant, circuit with the induction coil so that efficiency is maximized. The impedance matching of the electrical characteristics of the coil is accomplished through the use of an auto-transformer with multiple taps to select the voltage, and sufficient capacitance in 220, 440, and 800 volt banks to vary the frequency. With this arrangement, a wide range of coil sizes and configurations can be efficiently tuned.

7.1.3 Control Panel

The control panel has all the necessary switches, indicator lights and buttons that are required to operate the inverter and heat station. Two analog meters monitor voltage and frequency, and a digital meter monitors power output. The panel also has the controls needed to operate the recirculating water system, the quench chamber, compressed air for the blow-off chamber, and the chain drive motor.

7.1.4 Quench and Blow-off Chamber

The quench and blow-off chamber, see Figure 7, is built out of aluminum plate with acrylic windows in the front and back to allow visual inspection of the quenching process. The entire unit is mounted on

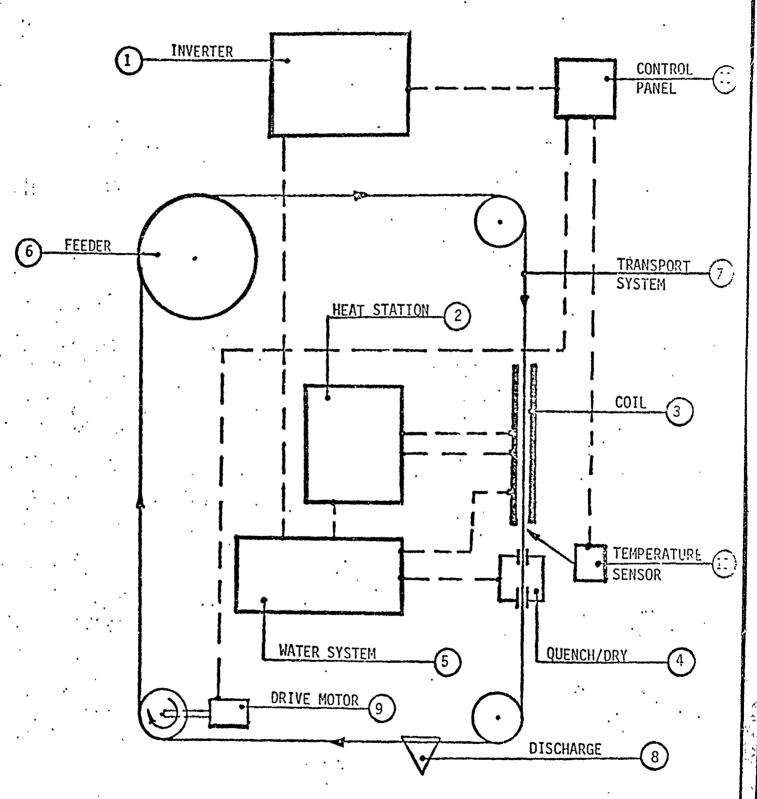
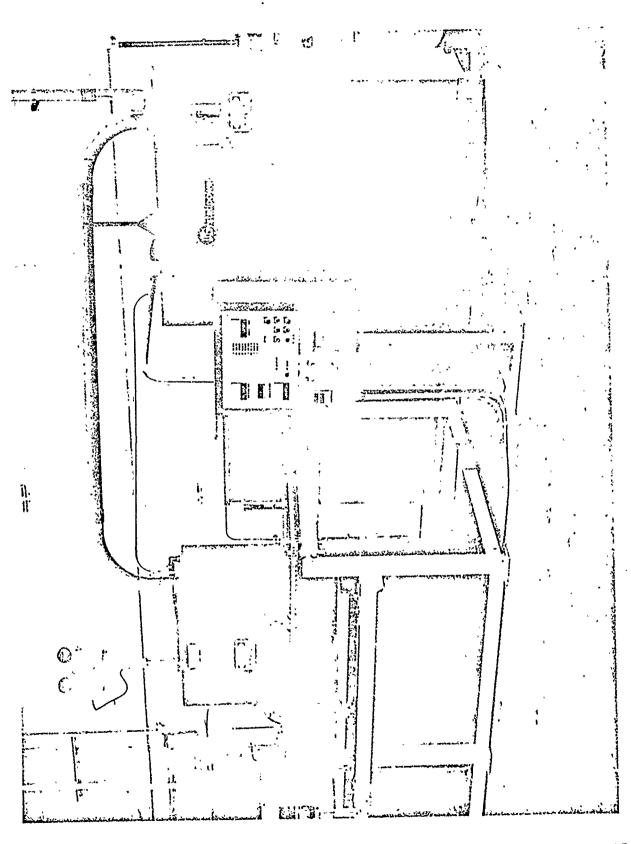
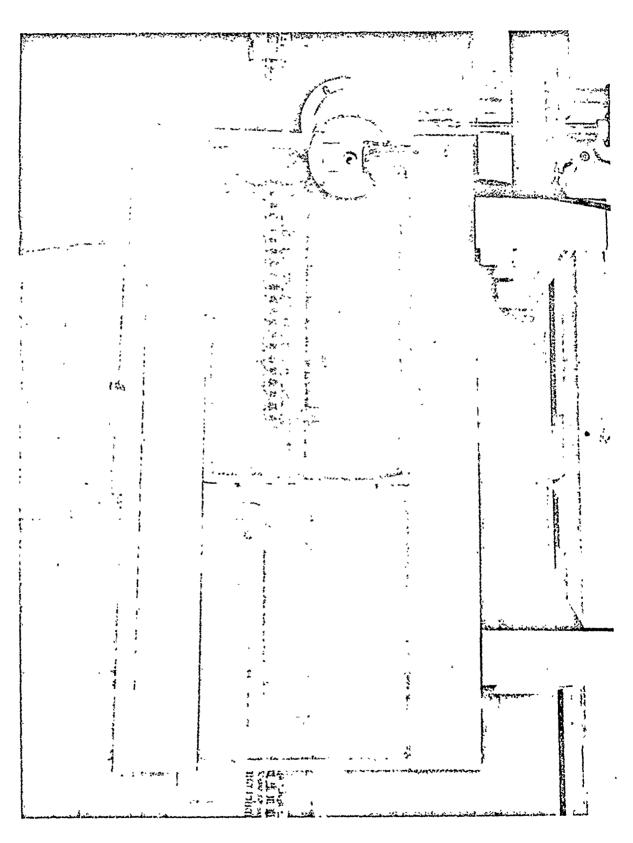


FIGURE 5 INDUCTION ANNEAL SYSTEM DIAGRAM



CARTRIDGE CASE QUENCH UNIT



moveable slides so that it can be moved toward or away from the coil. In this manner, the time required for full quenching can be varied to provide the optimum effect.

The quench chamber consists of a series of square-pattern spray nozzles arranged such that the cases are cooled quickly and uniformly. The blow-off chamber uses a series of wide-angle, flat-pattern air nozzles providing compressed air to dry the cases. All the nozzles are mounted in manifolds with a flexible connector so that they may be repositioned easily to accomodate the various annealing operations.

7.1.6 Transport System

Two 40-foot sections of nickel plated chain are used. The first chain has stainless steel pins on which the second draw parts are placed for the interdraw anneal operation. The second chain has beryllium copper clips which engage the extractor groove and is used for the body anneal, stress relief, and neck and mouth anneal operations. In both cases, part spacing is 0.75 inch and chain speed is 15 inches per second.

7.1.7 Accumulator Water System

An accumulator tank and a recirculating water system was incorporated to maintain constant cooling water temperature and pressure. The water from the inverter, heat station and coil is recirculated, but the water from the quench, which may wash off dirt, oxides or metal particles from the cases, is dumped into the drain to avoid contaminating or raising the conductivity of the recirculating water.

7.1.8 Principle of Operation

Although the tests were run on an intermittent basis, the characteristics of a continuous system were properly simulated. This was achieved by sandwiching the test pieces between quantities of non-test pieces. The purpose of the latter was to achieve coil load stability before the first test piece entered the coil, and maintain it until the last test piece exited.



Advanced Development and Engineering Center

With the 0.75 inch spacing and 15 inches per second chain speed, the simulated production rate was 1200 parts per minute.

7.2 Induction Coils

There are four coils used for the induction heat treating operations. These are:

- 1. interdraw anneal coil
- 2. body anneal coil
- stress relief coil
- 4. neck and mouth anneal coil

Each coil is a channel configuration with multiple turns (except for the single-turn neck and mouth coil). In this manner, each turn only heats a portion of the case so that reliance on conduction and the effects of ambient conditions are minimized, while efficiency is improved.

Each unit has positive and independent adjustment of the vertical and horizontal position of each turn to provide more predictable and repeatable results. The relatively short coil lengths also make it easier to adjust and align the assembly. The coils are mounted in box-type frames to provide a structure having rigidity together with visibility and accessibility. The top of this box assembly houses the chain guide as an integral part of the structure to ensure case-to-coil position accuracy.

Each coil is mounted on a wooden spacer to facilitate simple removal and installation. Each spacer is mounted on an adjustable tase plate to permit proper alignment of the coil assembly with the chain.

A list of coil drawings and a reduced copy of each assembly drawing is contained in Attachment 2.

7.2.1 <u>Interdraw Anneal Coil</u>

The interdraw anneal coil is two turns, 72 inches long and has iron lamination flux concentrators on the top turn. The entire top turn is utilized to heat the 1/4 inch point since the mass of metal in the base acts as a heat sink. The iron laminations direct and concentrate the lines of flux into this area. The bottom turn is slanted slightly to heat the rest of the case. The material for the case guide is a silicone/glass laminate that is nonconductive, withstands high temperatures, and has fairly good wear properties.

7.2.2 Body Anneal Coil

The body anneal coil is three turns and is 36 inches long. As with the interdraw anneal coil, the top turn is used solely to heat the 1/4 inch point, with the other two turns heating the rest of the case.

7.2.3 Stress Relief Coil

The stress relief coil is four turns and is 18 inches long. During the stress relief operation, the cases are heated to about $600^{\rm O}{\rm F}$ to remove any residual stresses.

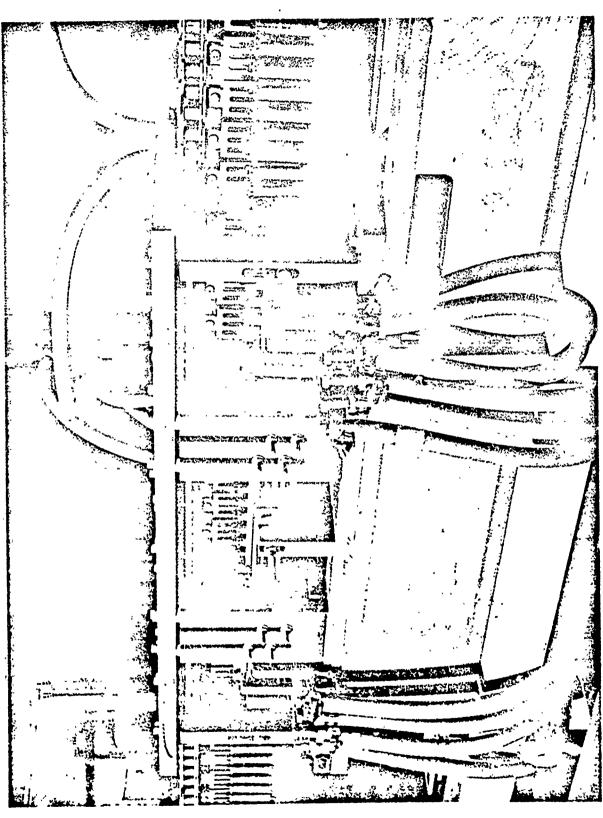
7.2.4 Neck and Mouth Anneal Coil

The neck and mouth anneal coil is a single turn and is 18 inches long. This coil is used to anneal only the 1-7/8 inch point, whose hardness was raised significantly in the tapering operation. The neck and mouth anneal also imparts the iris on the mouth of the case. A typical coil assembly is shown in Figure 8.

CARTRIDGE CASE INDUCTION COIL ASSEMBLY

ω

FIGURE



7.3 Final Configuration

As with the tooling, the anneal development was an iterative process carried out until the desired characteristics were achieved. The final coil settings are included on the appropriate assembly drawing. It should be noted that the settings should be used only as a guide. Other adjustments may be used depending on ambient conditions, water cooling effectiveness and changes in workpiece characteristics caused by tool wear.

Hardness readings were taken on a Wilson Tukon Hardness Tester and grain structures were observed using a Bausch and Lomb metallograph.

7.3.1 Interdraw Anneal

The objective of this development was to satisfy the specified grain structure on the final case. The specification is comparative in nature, with the actual grain size having to fall between a minimum and a maximum (as defined by reference photomicrographs) at each location.

It was found that no discernible grain distortion occurred in final draw or subsequent operations.

The only unexpected factor was that the required power output was 216 KW. This was 108% of the induction unit rating of 200 KW which was originally estimated to be adequate. Such a condition would be undesirable on a long term basis. However, the unit is basically a 250 KW model de-rated and could easily be upgraded to its normal rating.

7.3.2 Body Anneal

Consistent with previous experience, fulfillment of hardness gradient specifications was a time consuming process.

Power required was 112 KW.

7.3.3 Stress Relief

This operation is such that coil and power settings are not critical.

7.3.4 Neck and Mouth Anneal

The main problem encountered here was in maintaining an even and consistent iris. It is believed that the major cause was inconsistency of cleaning prior to the anneal and that this condition would not apply in a properly functioning production process.

Power required was 98 KW.

Recommended hardness profiles following the various anneals are shown with the in-process data of Section 8.

Note that these profiles are advisory only.

7.4 Void Test

Five tests were performed to evaluate the effects of voids (missing cases) on the ability of the annealing system to correctly heat treat the 7.62 mm cases. The five tests were performed in compliance with contract DAAK10-78-C-0165 modification P00001, and are repeated here for the convenience of the reader:

- A. All twenty-four stations filled. Hardness data to be used as base line for Test B and D.
- .B. Four voids spaced evenly throughout the twenty-four station positions on the chain. Anneal power to be adjusted to the base line hardness data established in Test Condition A.
- C. Four consecutive voids in the twenty-four station positions on the chain. Anneal coil power setting to be the same as used in Test Condition B.
- D. Six voids evenly spaced throughout the twenty-four station positions on the chain. Anneal coil power to be adjusted to the base line hardness data established in Test Condition A.
- E. Six consecutive voids out of the twenty-four station positions on the chain. The anneal coil power settings to be the same as used in Test Condition D.

Each test was run five times and six samples were taken from each test. The 1/2 and 1-1/2 inch points were checked for hardness on each of the 150 test pieces. To obtain results that reflected the worst possible condition, the samples were taken from the positions immediately adjacent to the voids. For example, in test (C), three groupings of 24 cases were run with a void of four missing cases in the middle of each group. Therefore, if each set was numbered 1 to 24, the cases in the position of 11 to 14 were removed to act as the void, and the cases in the positions of 10 and 15 were removed from each group as the test samples.

The results are summarized in Attachment 7, with the hardnesses given for each test being the average of 30 cases.

Because of the large number of samples and the time consuming nature of reading hardness, measurements were limited to the $\frac{1}{2}$ inch and $1-\frac{1}{2}$ inch locations.

By comparing tests A, B and D, it is seen that the evenly spaced voids can be stabilized at the correct hardness by power adjustment to well within experimental scatter.

On the other hand, comparing C with B, it is seen that the A consecutive void arrangement produces a severe drop in hardness at the $\frac{1}{2}$ inch location of about 26 DPH, and very little change at the $1-\frac{1}{2}$ inch location.

As may be expected, the condition is worse with 6 consecutive voids (comparing E with D), which produces a hardness drop of about 40 DPH at the $\frac{1}{2}$ inch location and a slight drop at the $1-\frac{1}{2}$ inch location.

8. IN-PROCESS PART DEFINITIONS

As mentioned in section 6, the program began with tentative in-process specifications. As with the tooling, minor changes were made as the process development progressed. The final recommended definitions not covered by the L.C.A.A.P. in-process or final case dimensions are included as Attachment 3.

Also included for reference are copies of the cup drawing 10522459 and the case drawing 10521997.

9. FINISHED PART INSPECTION

A small random sample from the same batch as the 1,000 parts supplied to ARRADCOM was inspected for compliance to the required specifications.

9.1 <u>Dimensional</u>

Measurements are made on the in-process parts and on the finished cases. The resulting data is included in Attachment 4.

9.2 Metallurgical

Measurements of external surface hardness and internal head hardness, together with typical microphotographs of grain structure are included as Attachment 5.



10. TEST FIRINGS

A small sample from test series C was submitted to H.P. White Laboratory Inc. for test firing. They were loaded to M80 high pressure test specifications and fired in a pressure barrel. No deficiencies were noted in the subsequent inspection.

The test report is included as Attachment 6.

11. SCAMP EQUIPMENT CHANGES

11.1 Tooling

SCAMP tool modules were used throughout. Relative to 5.56 mm production, the additional draw operation was accomplished by using a standard first draw module and equipping it with second draw tooling; the pre-pocket tooling was installed in a standard header module.

The only change made in the tool module area related to non-metalworking components involved draw punch alignment. Test series A and B had shown some difficulty in maintaining wall thickness variation tolerance of the final draw part. Investigation showed this to be caused by punch-to-die misalignment. This, in turn, resulted from the restricted length of the punch shank-to-gland-to holder engagement and the clearances involved, which induced the misalignment when the retaining nut was tightened.

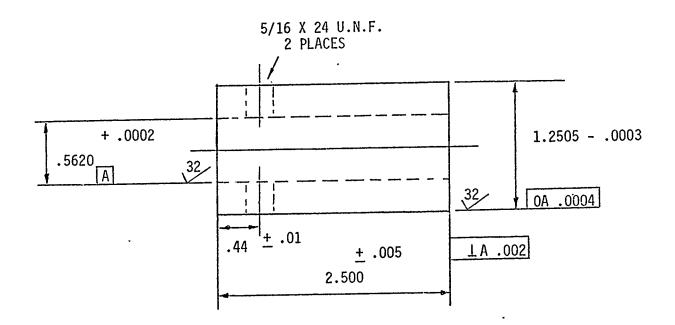
This condition was corrected by installing a re-designed sleeve which maximized engagement length. This modification is shown in Figure 9.

It may be noted that the sensitivity to misalignment is not present in the existing G+W 7.62 mm two-draw process which uses a cup with greater height: diameter ratio.

11.2 Basic Equipment

Relative to the 5.56 mm SCAMP case sub-modules operating at L.C.A.A.P., additions to the basic equipment would be provisionally as follows:

- 1. Draw press to perform the additional draw operation.
- 2. Additional drive motor and control system.
- 3. Interdraw anneal station consisting of 250 kw power unit, heat station, coil assembly, wash station, quench and blow-off stations, plus entry and exit re-spacers.
- 4. Header press to perform the pre-pocket operation.
- 5. Two transfer turrets to correct the pass-line changes introduced at the additional draw and pre-pocket presses.



MATERIAL
PRE-HEAT TREATED
4130 Rc28 - 32 or Equivalent

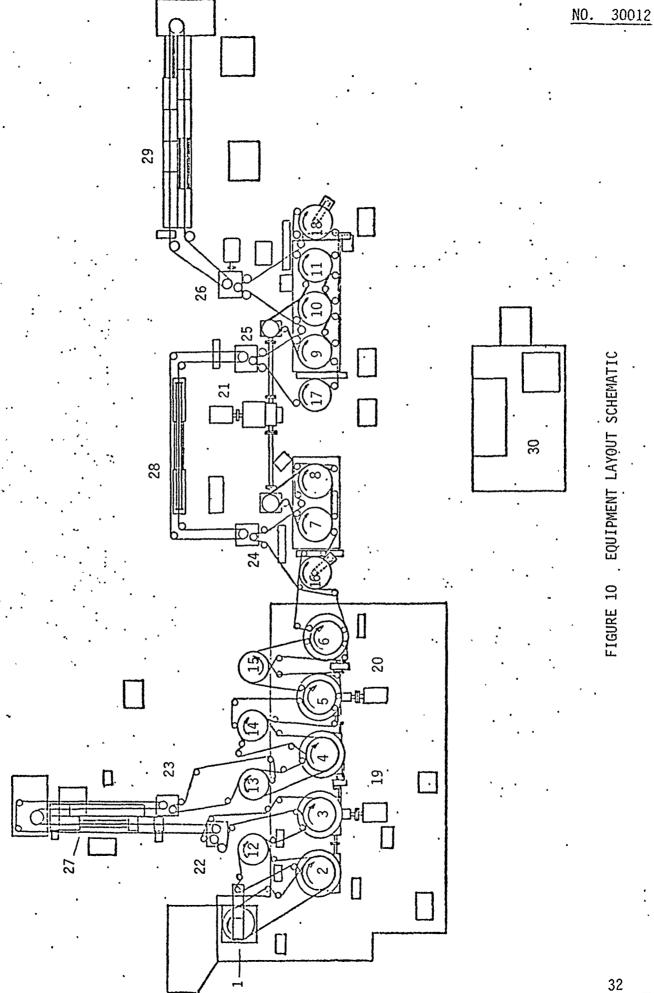
FIGURE 9 DRAW PUNCH SLEEVE

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11.3 Layout

A possible equipment layout is shown schematically in Figure 10. In practical terms, location of the two additional presses could be most effectively provided for by excavation of the existing pit. The pit does have one "spare" station, so that excavation would be limited to extension by one station upstream.

The details of the sub-module changes, such as drive re-arrangement, provision of transport system supports and utilities are properly the subject of a study beyond the scope of this contract.



EQUIPMENT LAYOUT SCHEMATIC FIGURE 10

32



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<u>Key</u>

- 1. Cup Feeder
- 2. Initial Draw Press
- 3. Second Draw Press
- 4. Final Draw Press
- 5. Pre-Pocket Press
- 6. Header Press
- 7. Head-Turn Press
- 8. Pierce Press
- 9. First Taper Press
- 10. Second Taper Press
- 11. Trim Press
- 12. Eject-Transfer Turret
- 13. Eject-Transfer Turret
- 14. Eject-Transfer Turret
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- 17. Eject-Transfer Turret
- 18. Eject-Transfer Turret
- 19. Drive Motor
- 20. Drive Motor
- 21. Drive Motor
- 22. Re-Spacer
- 23. Re-Spacer
- 24. Re-Spacer
- 25. Re-Spacer
- 26. Re-Spacer
- 27. Interdraw Anneal Station
- 28. Body Anneal Station
- 29. Stress Relief Anneal, Neck & Mouth Anneal, & Clean Station

FIGURE 10 EQUIPMENT LAYOUT SCHEMATIC (Continued)

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12. CONCLUSIONS

The program has demonstrated the feasibility of producing 7.62 mm M80 cartridge cases to U.S. N.A.T.O. specifications on a SCAMP sub-module at 1200 parts per minute.

All final case dimensional and metallurgical specifications can be fulfilled without exception.

A critical factor in the process was the successful development of induction heating to stimulate re-crystallization and grain growth with a continuous work-piece flow in less than 5 seconds.

All tools are compatible with existing tool modules and sub-module presses and their fabrication requires only normal techniques.

Because of the stipulated use of the standard U.S. cup and incorporation of a pre-pocket operation, two additional presses are required and excavation of the pit will be necessary.

Logically, this program should be followed by a design study which would be aimed at developing a realistic layout of the converted sub-module.

30012

Advanced Development and Engineering Center

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TOOL DRAWINGS ATTACHMENT 1

First Draw	
Punch	11831357
Bottom Die	11831578
Middle Die	11831579
Top Die	11831360
Stripper	11831361
Retainer	11831362
Second Draw	
Punch	11831364
Bottom Die	11831365
Middle Die	11831366
Top Die	11831367
Stripper	11831368
Retainer	11831369
Third Draw	
Punch	. 11831371
Bottom Die	11831372
Middle Die	11831373
Top Die	11831374
Stipper	11831375
Stripper	11831376

Retainer

11831377



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Poc	ke	t

 Stem
 11831379

 Bunter
 11831381

Head

 Stem
 11831384

 Bunter
 11831385

Pocket/Head

Die 11831380 Retainer Nut 11831382

Head Turn

 Mandrel
 11831387

 Form Tool
 11831388

 Stripper
 11831389

 Guide Roller Pin
 11831390

 Plug
 11831391

 Guide Holder
 11831392

 Guide Roller Assembly
 11831393

<u>Pierce</u>

 Punch
 11831395

 Guide Punch
 11831396

 Stem
 11831397

 Stripper
 11831398

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First Taper

 Body Die
 11831400

 Shoulder Die
 11831401

 Mandrel
 11831402

Second Taper

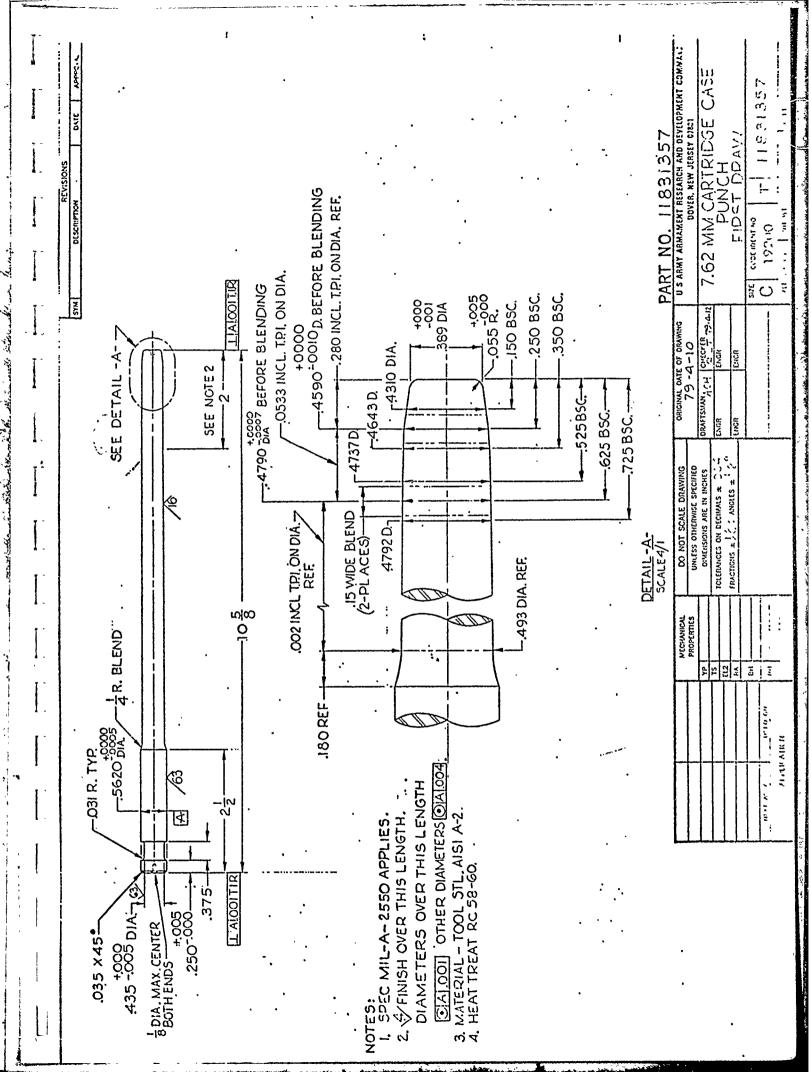
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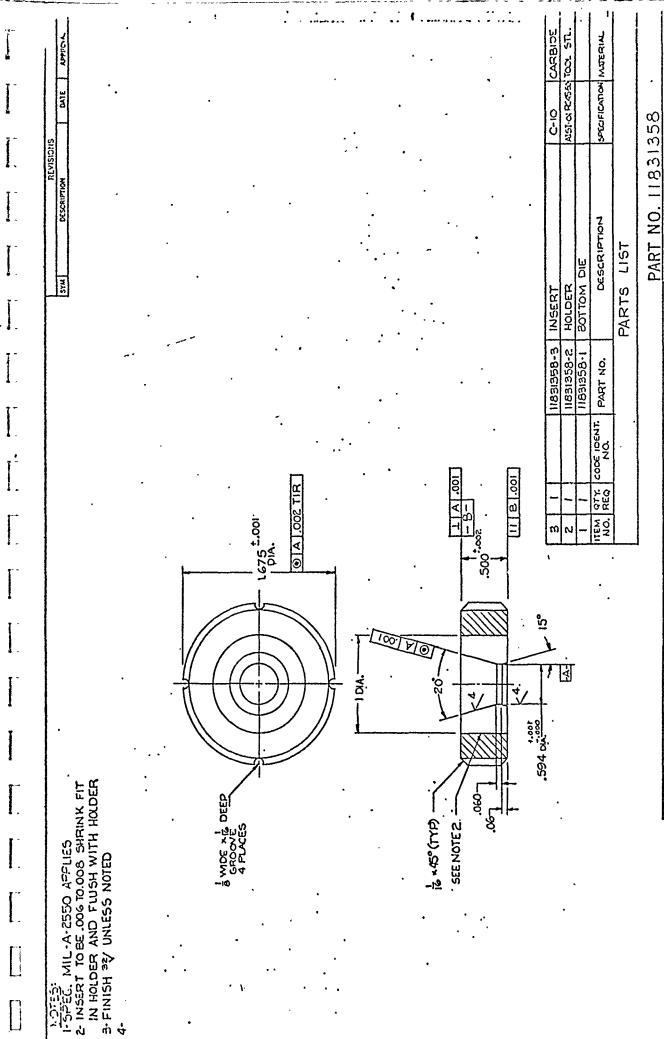
 Shoulder Die
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 Mandrel
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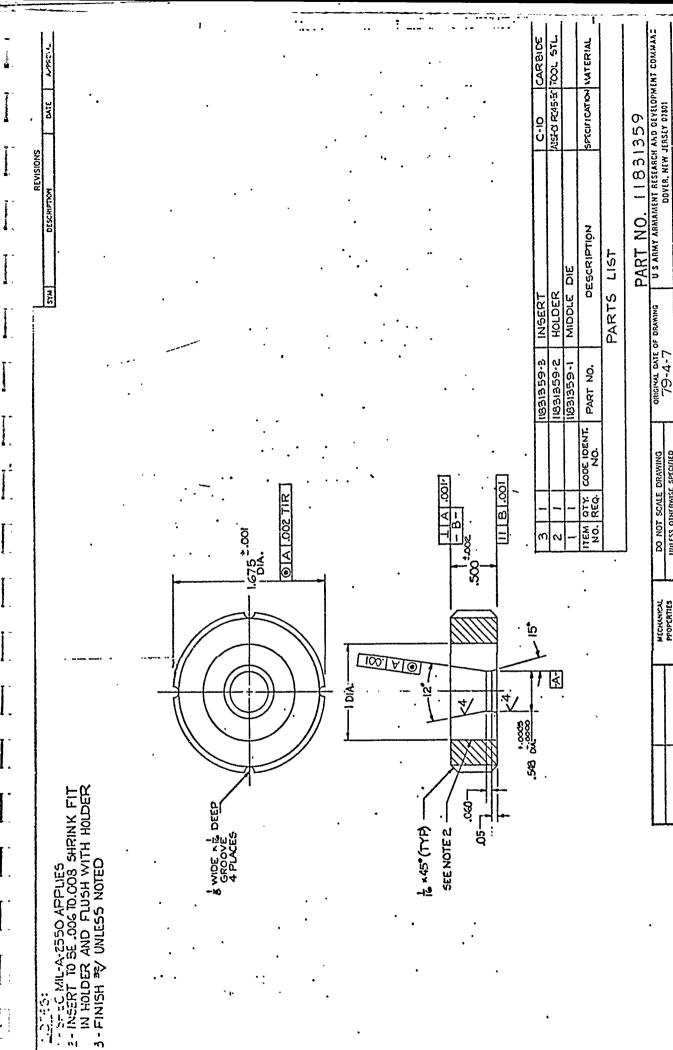
First/Second Taper

Mandrel Seat 11831 406 Sleeve 11831 407





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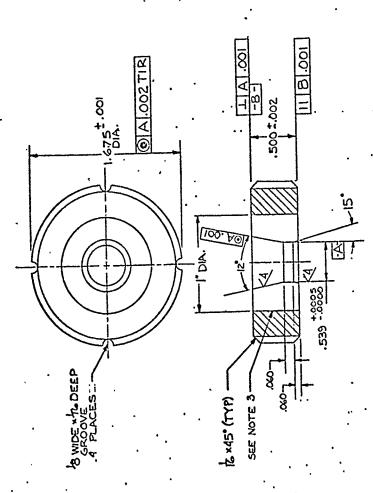
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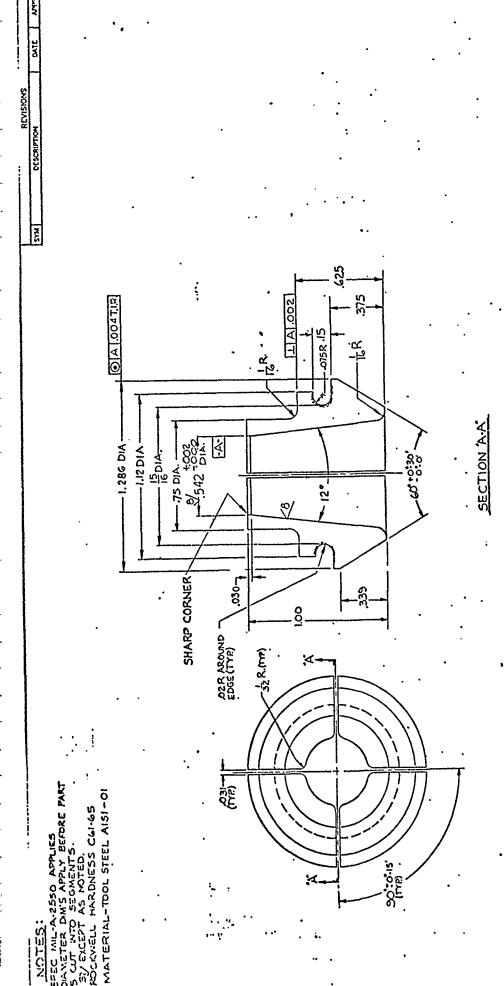
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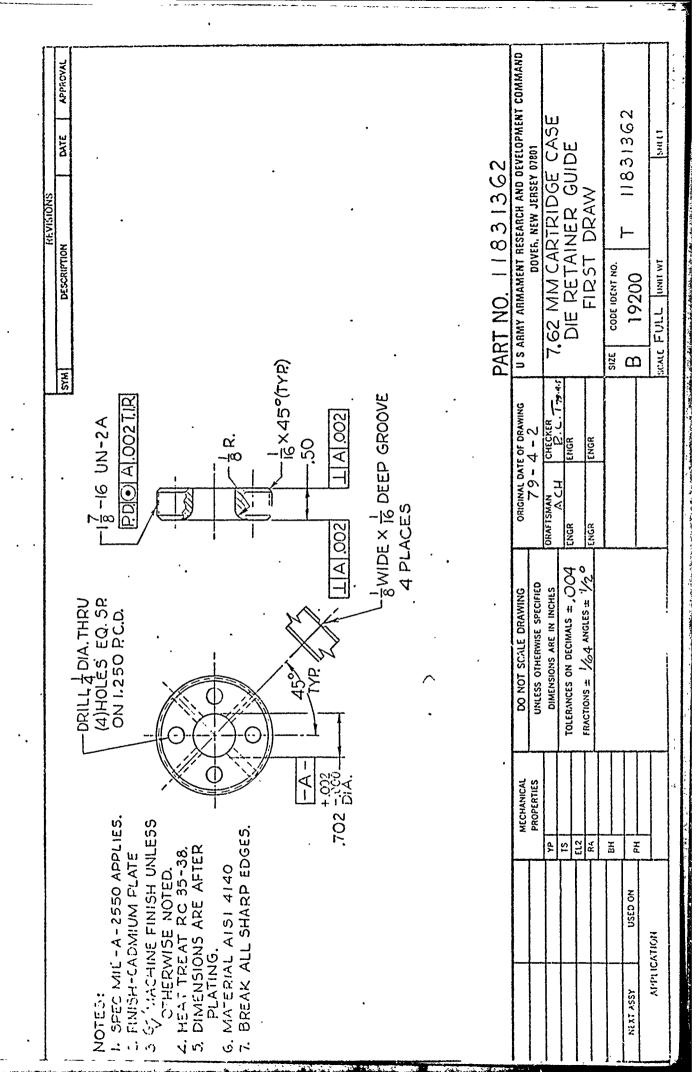
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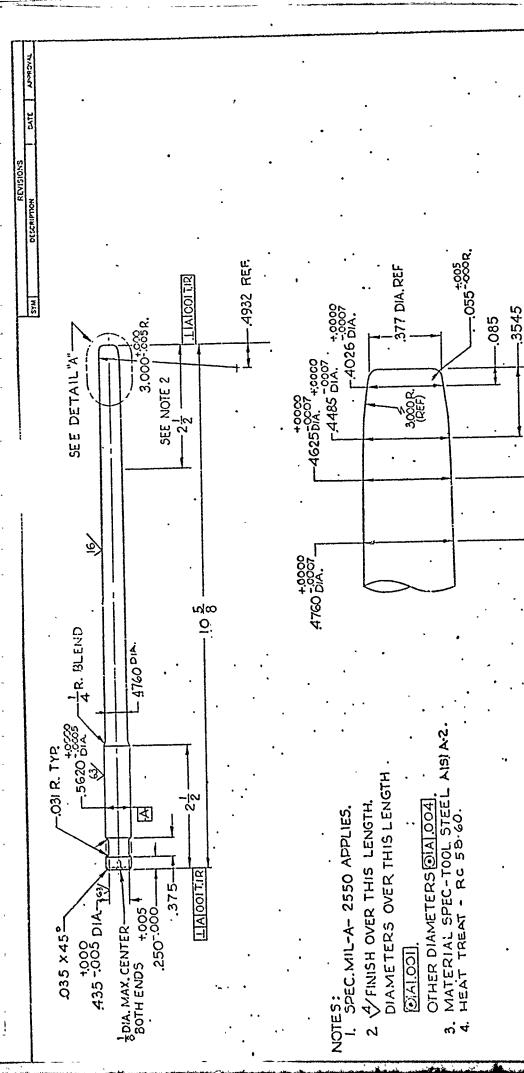
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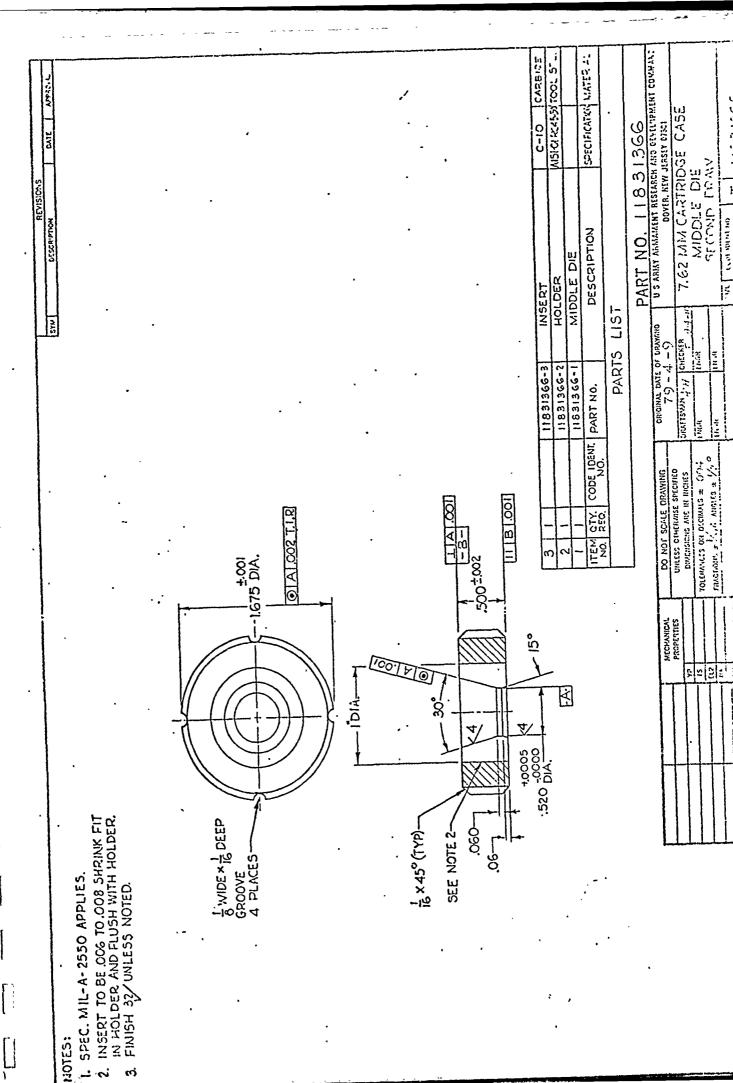
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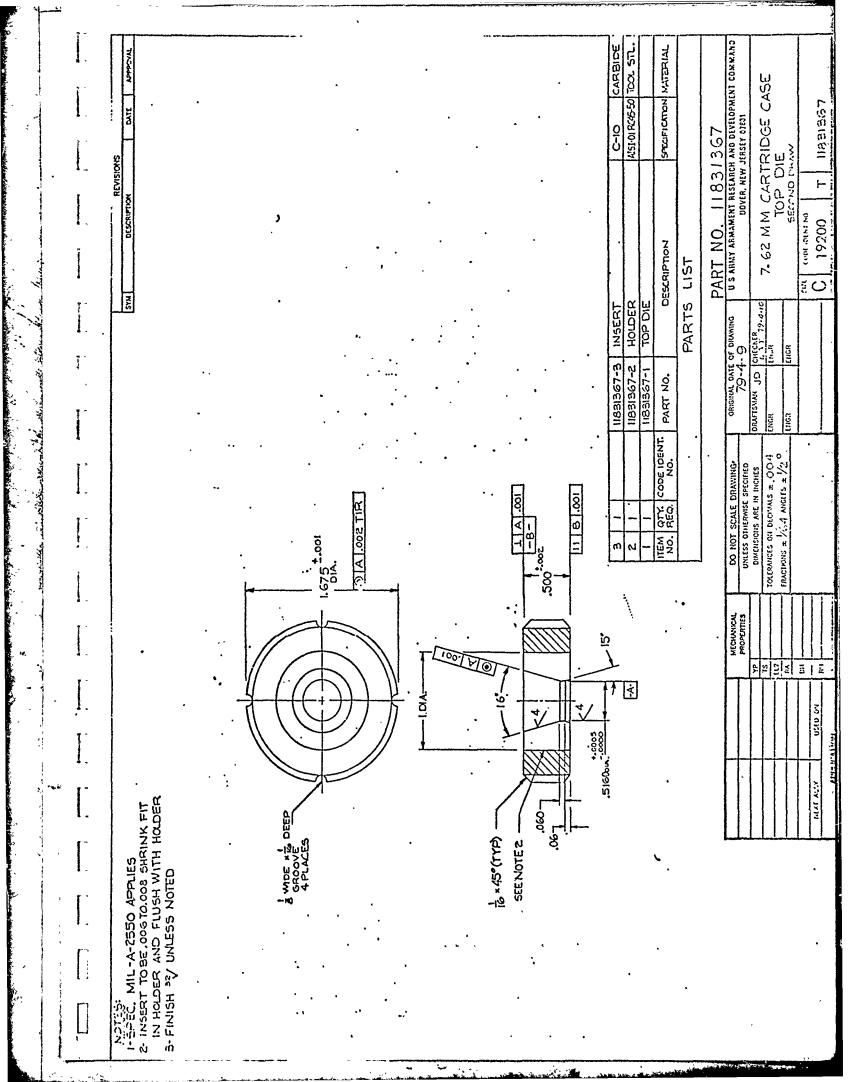
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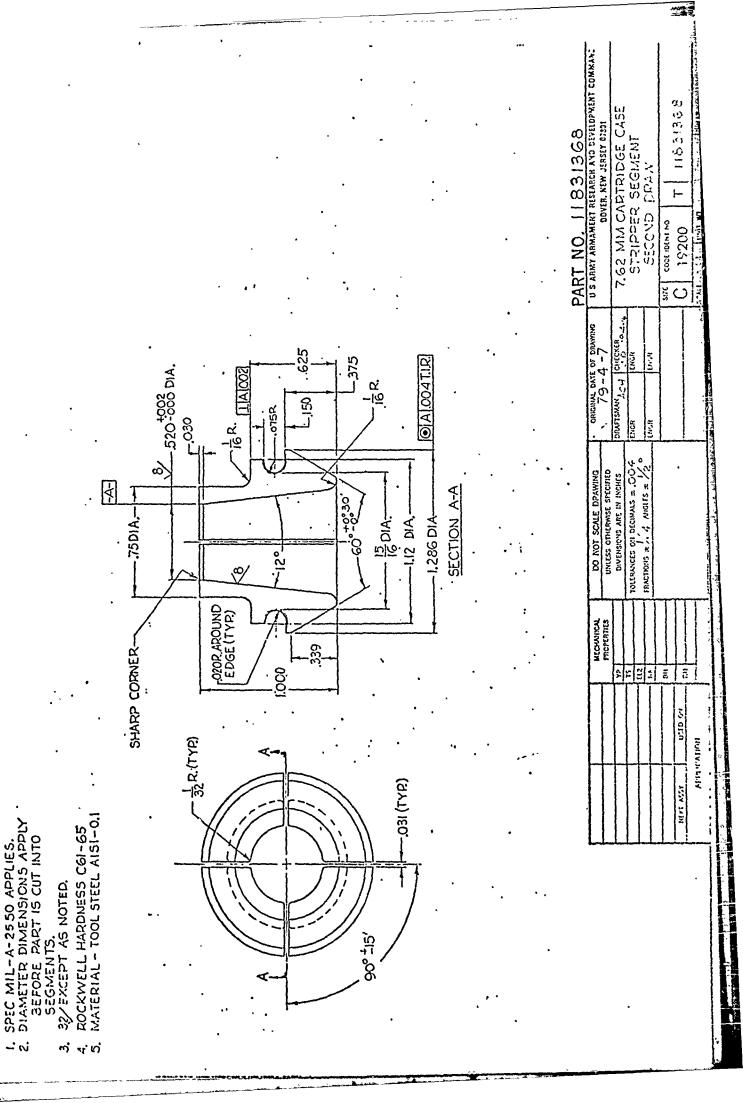
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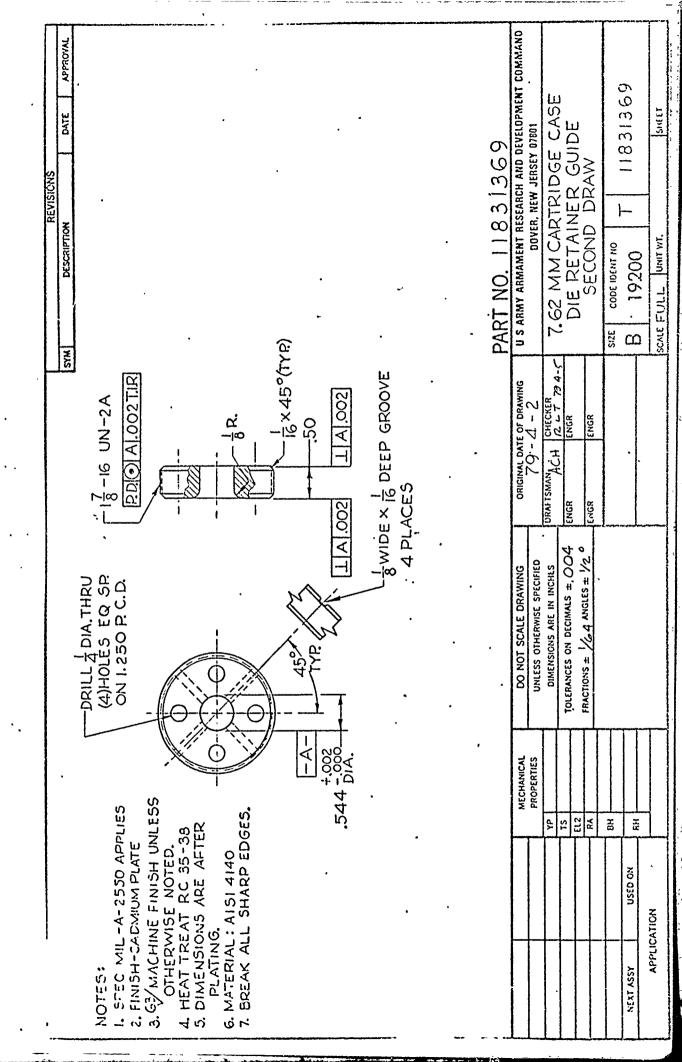


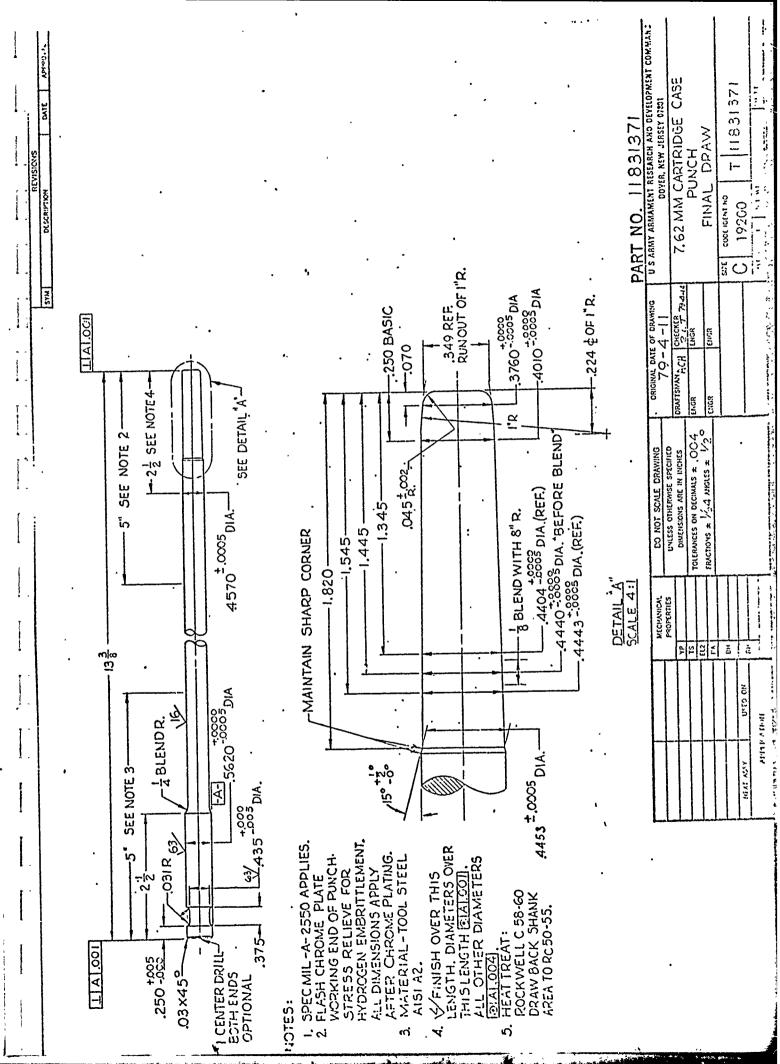
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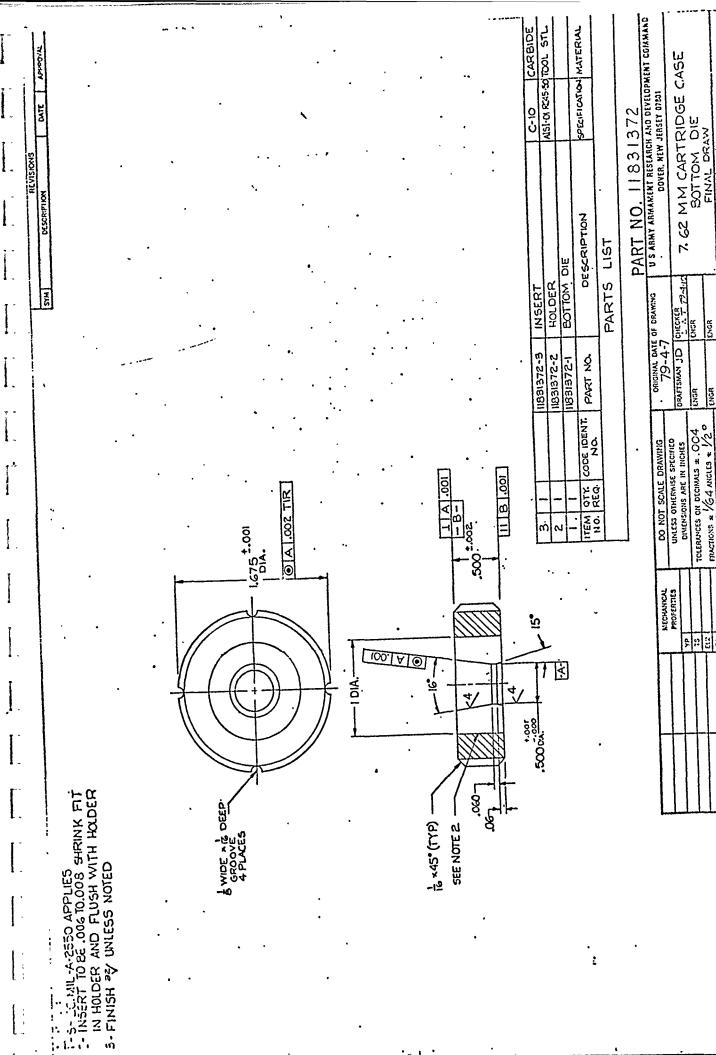




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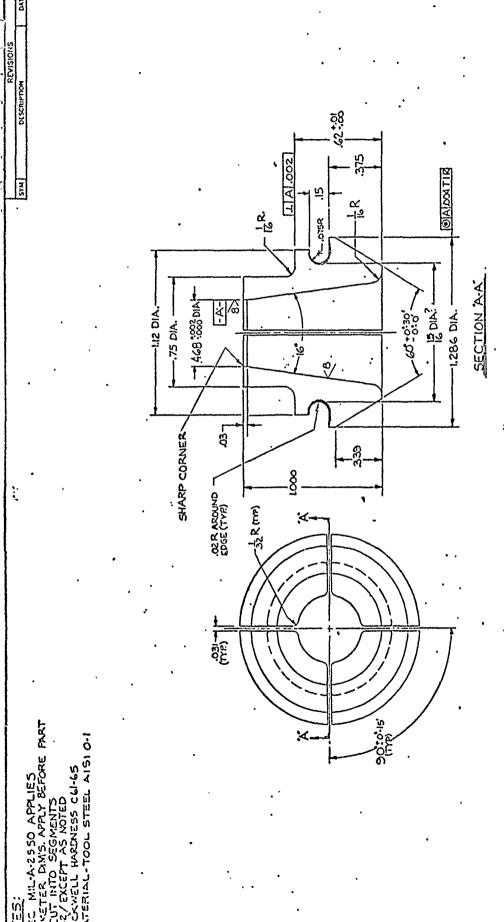
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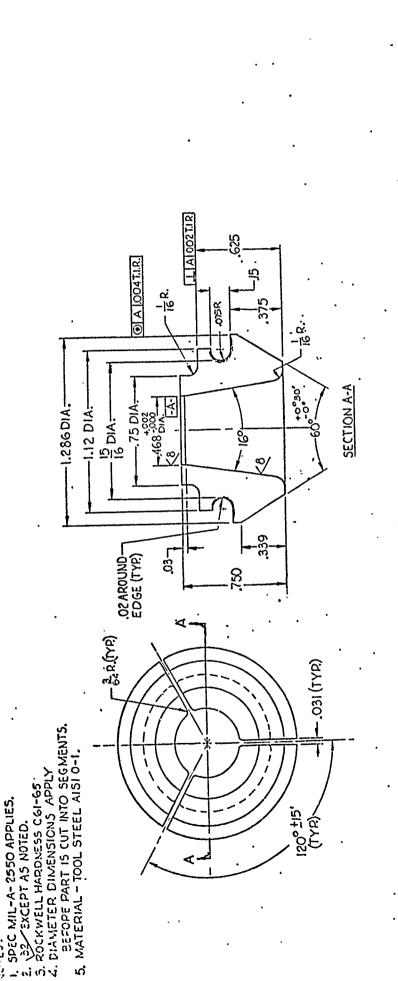
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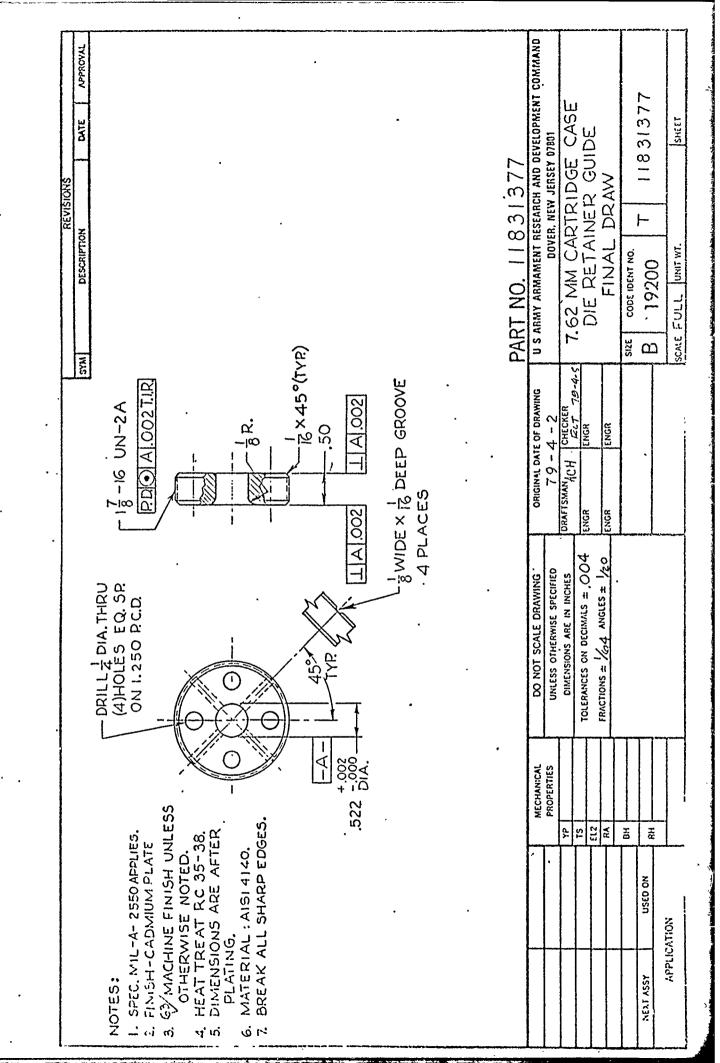
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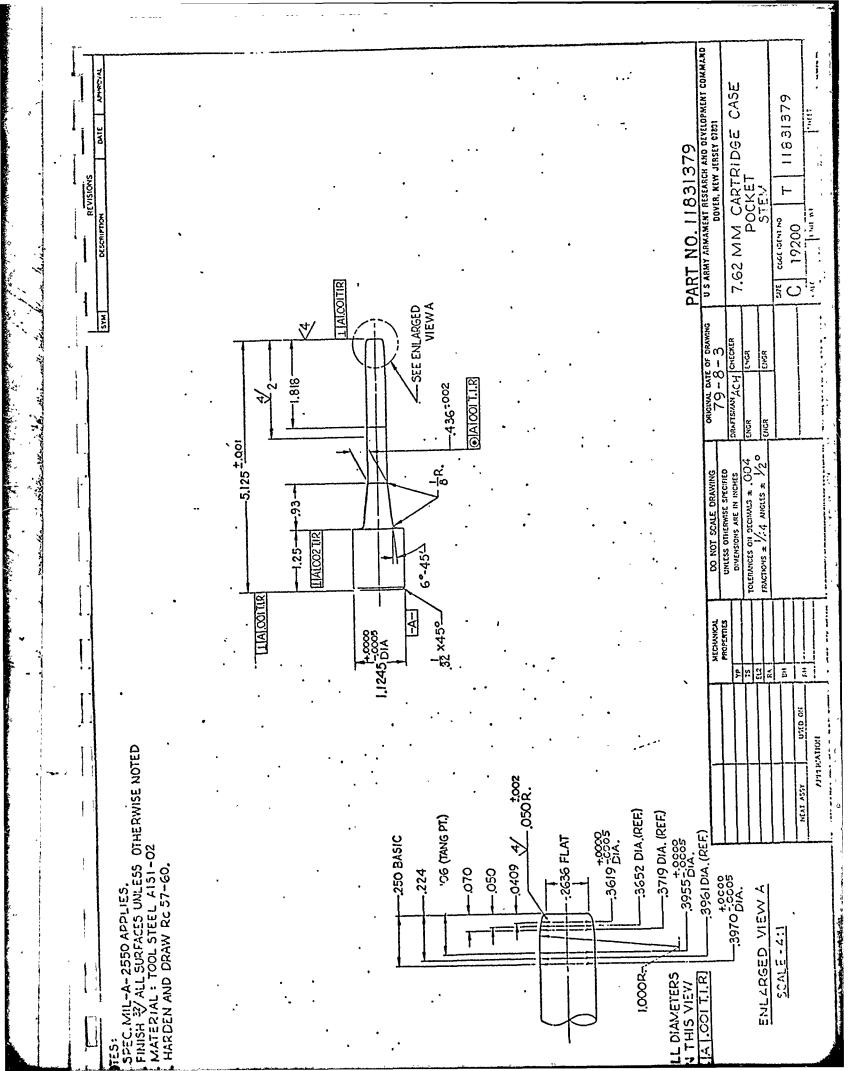
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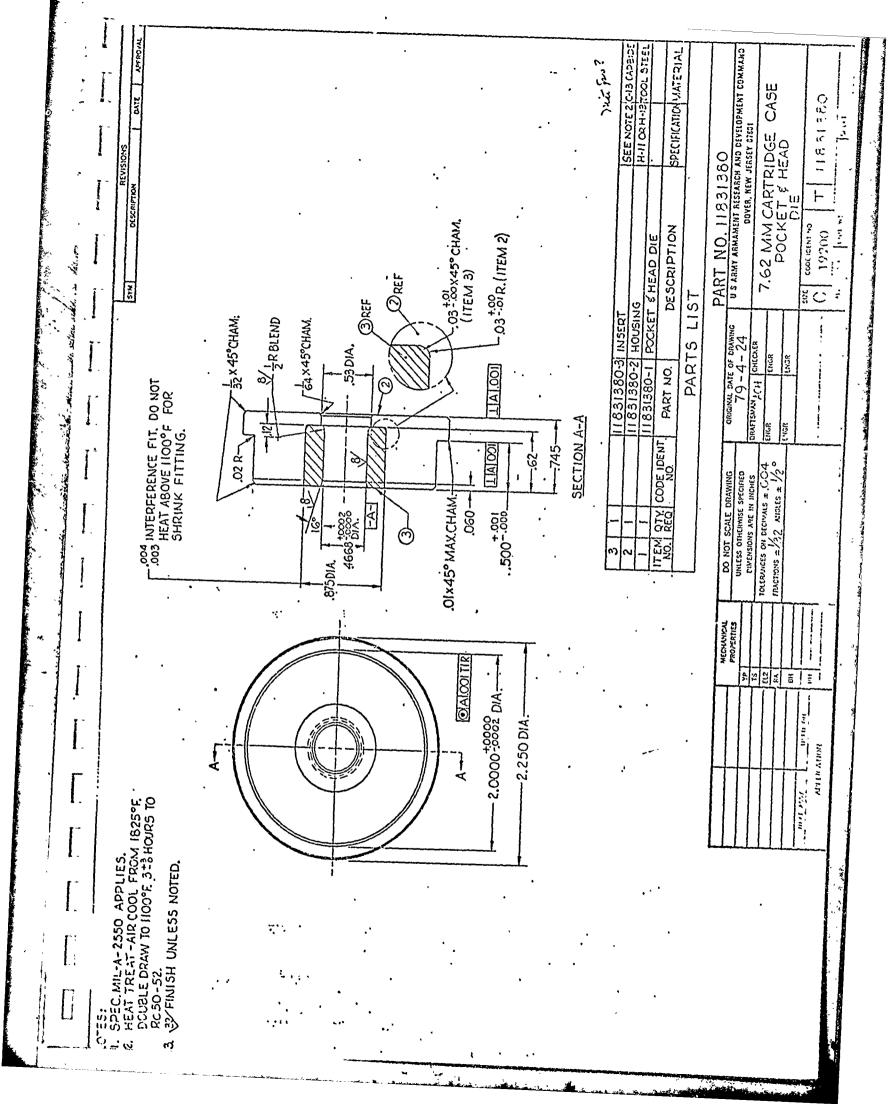


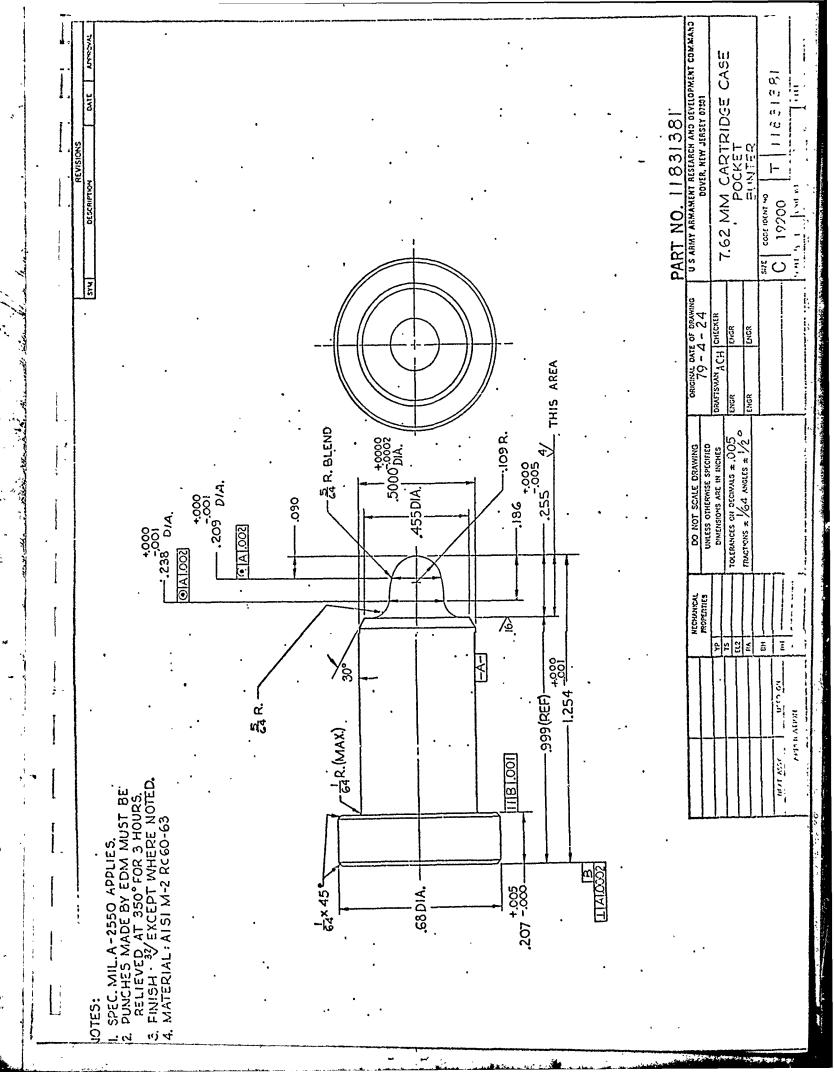
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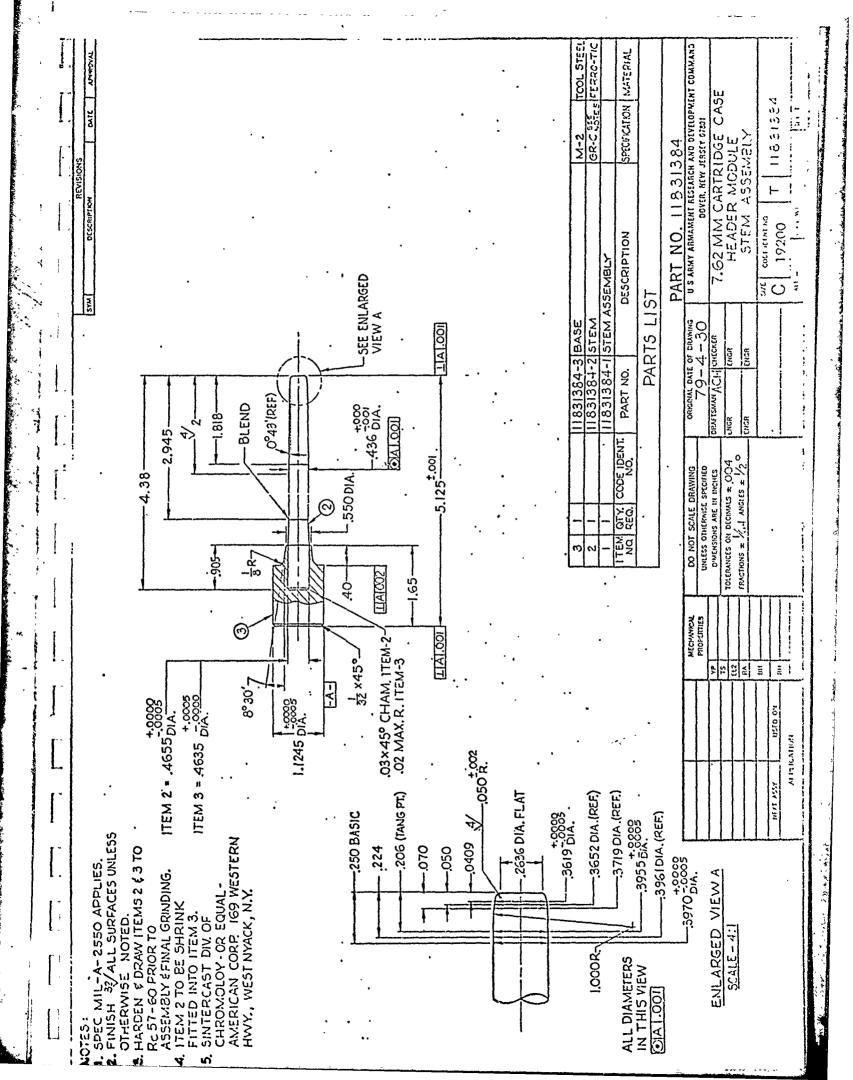


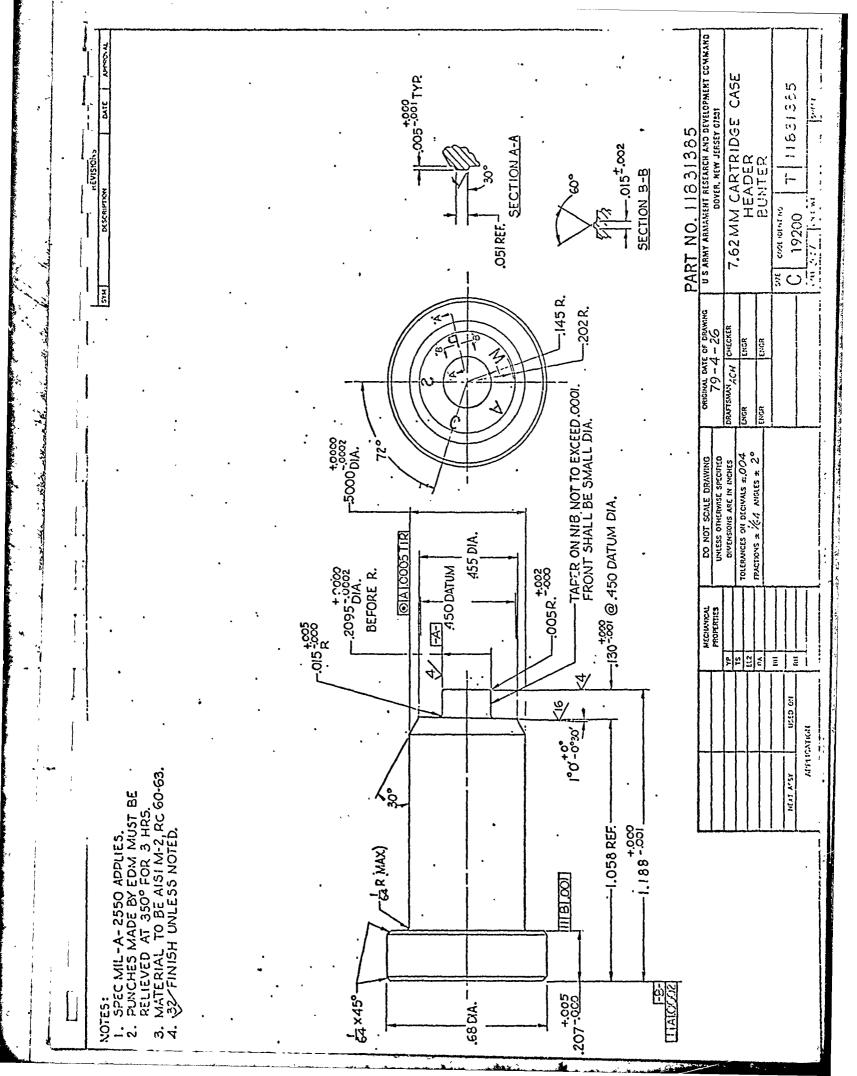
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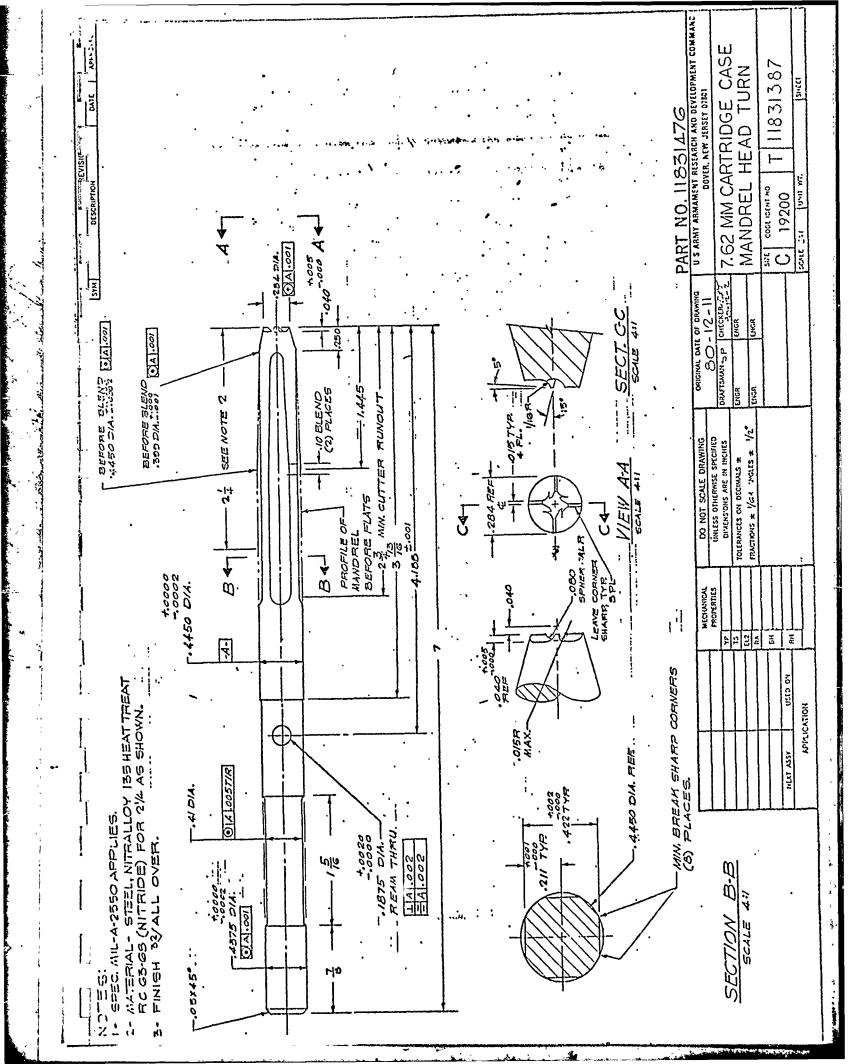
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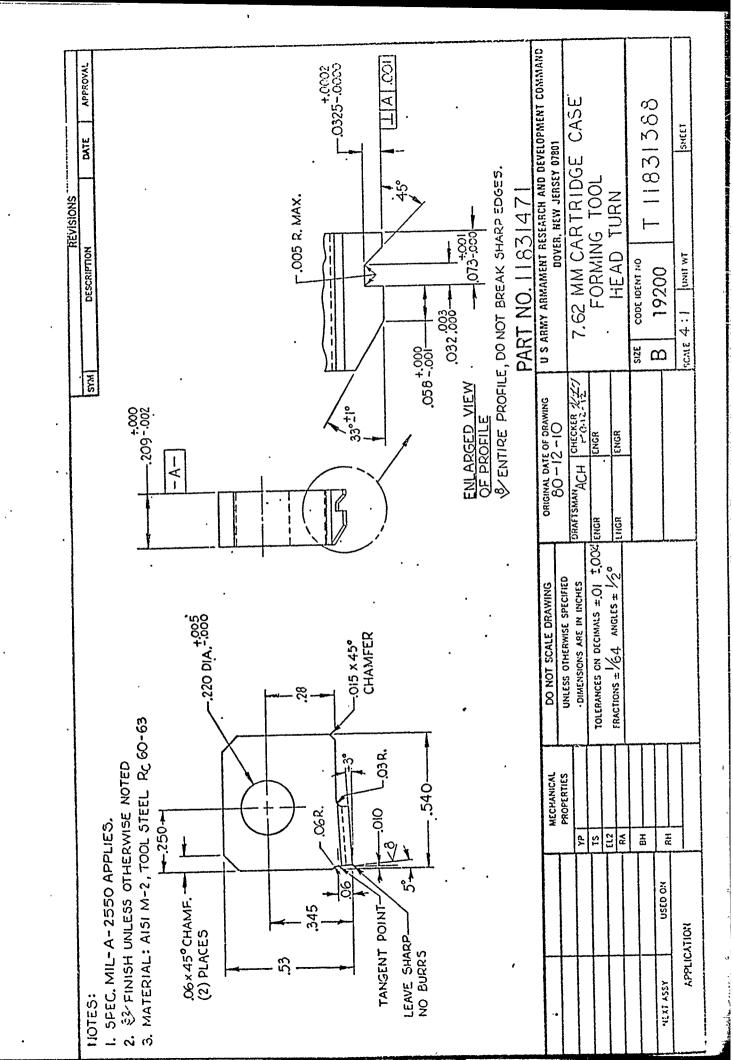
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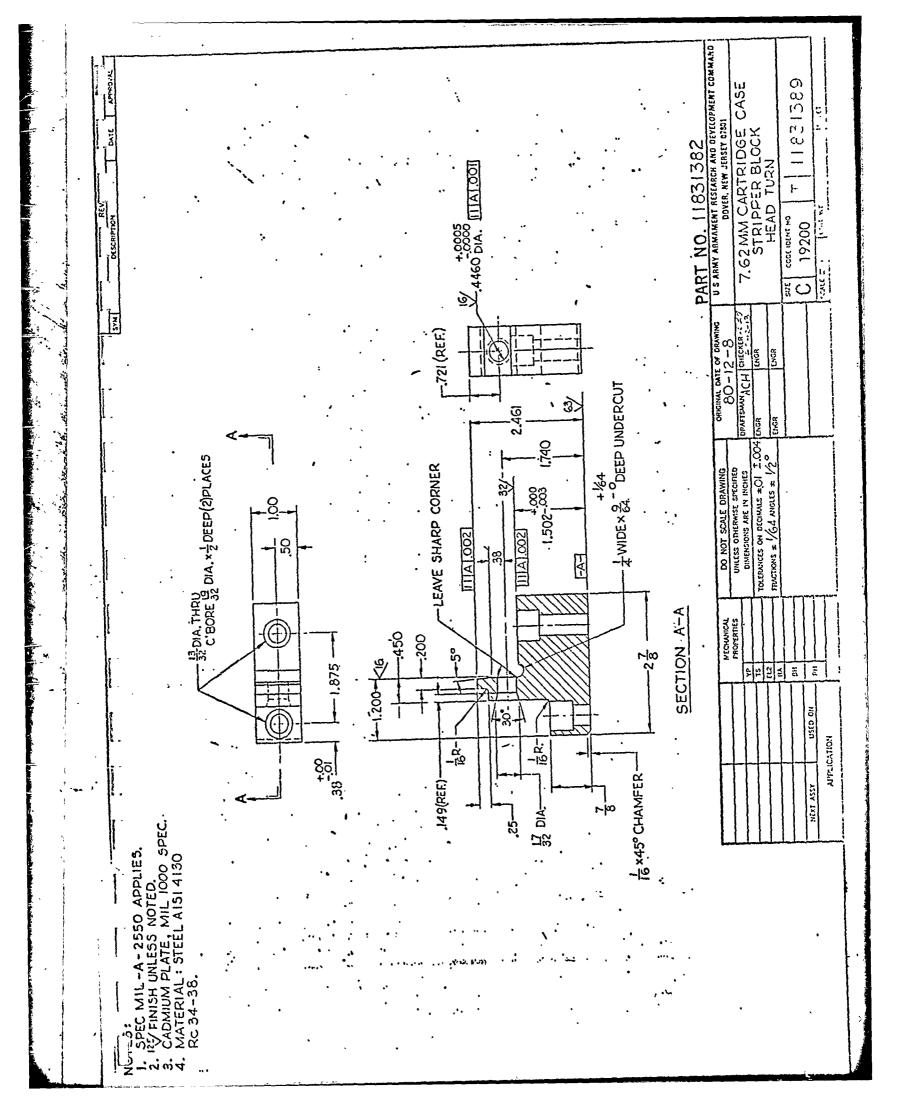
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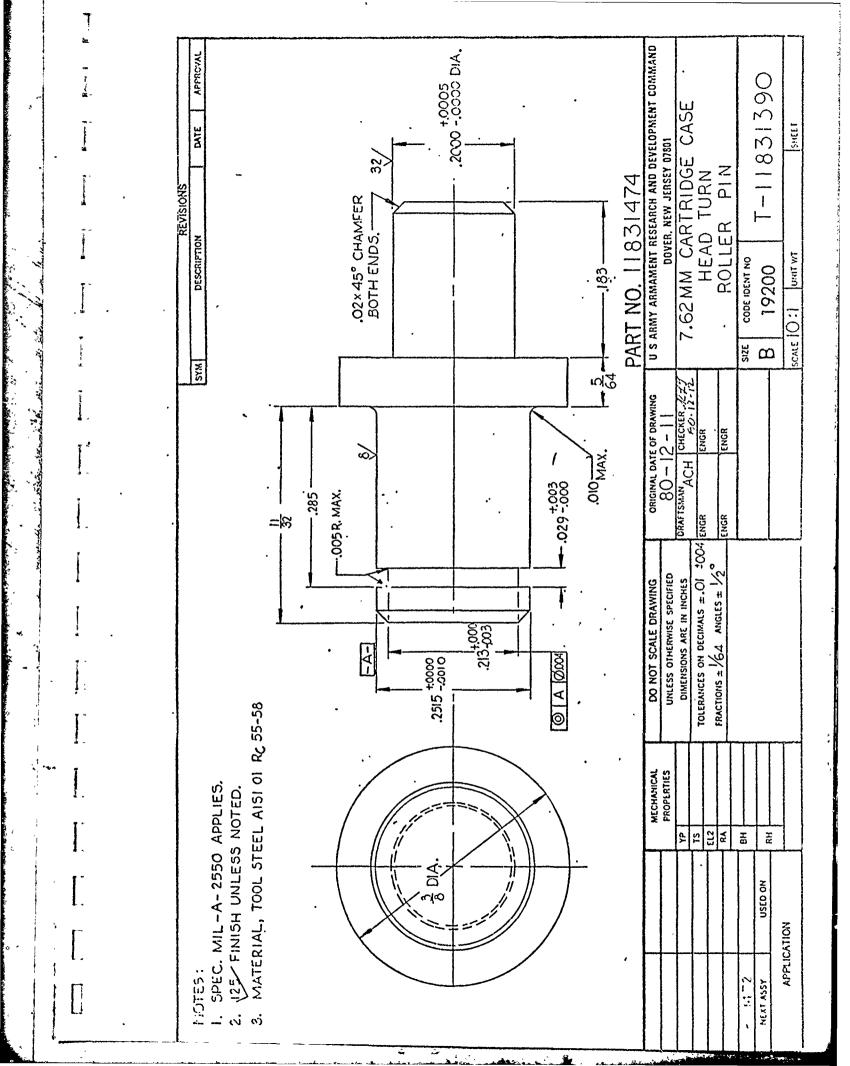


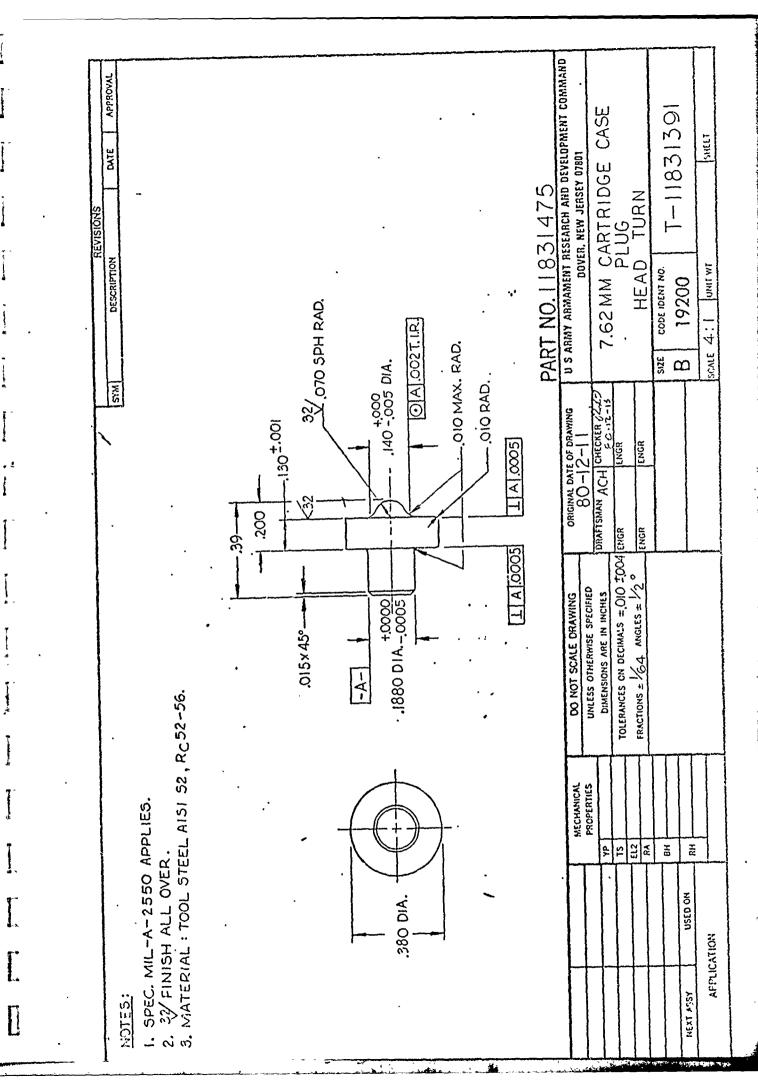


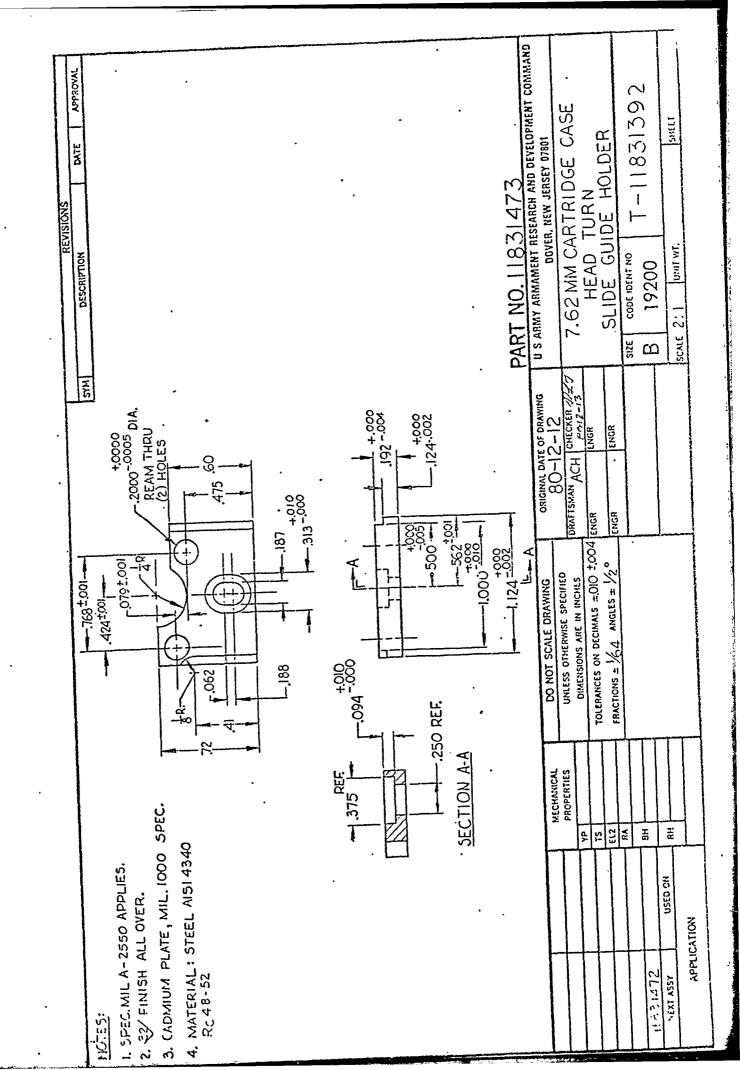


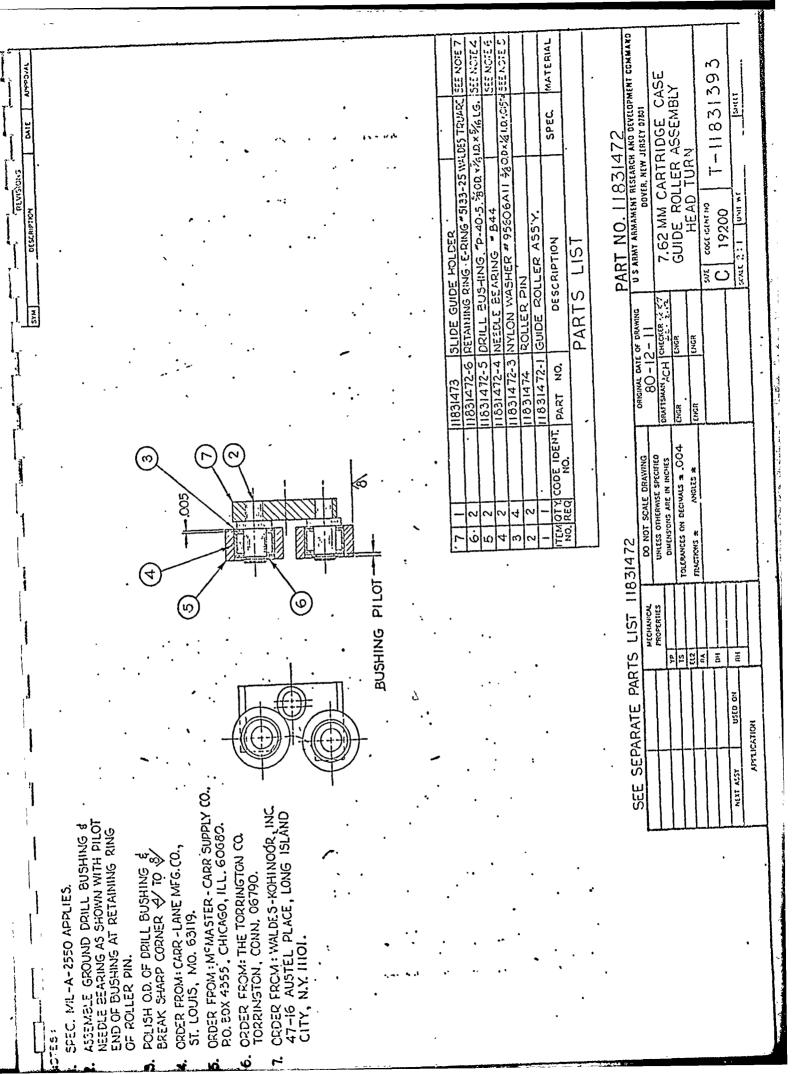


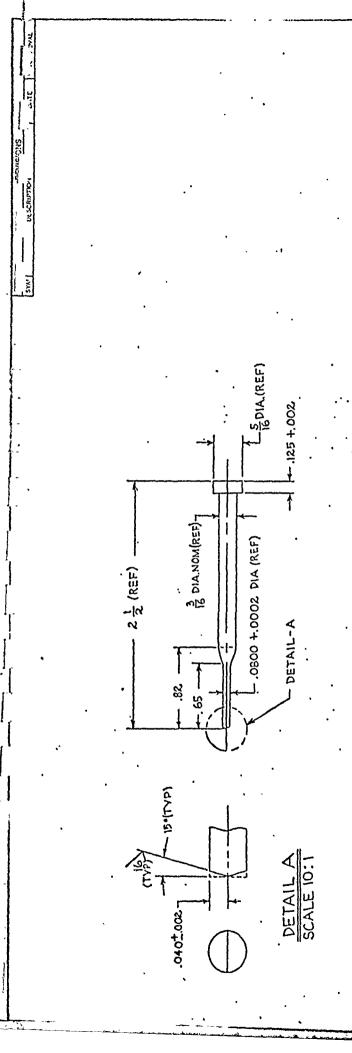






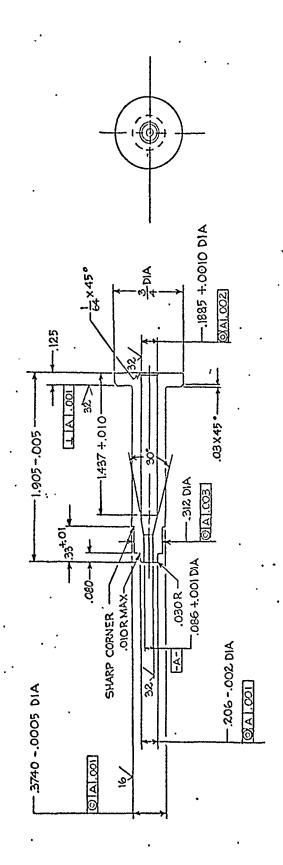






NOTES:
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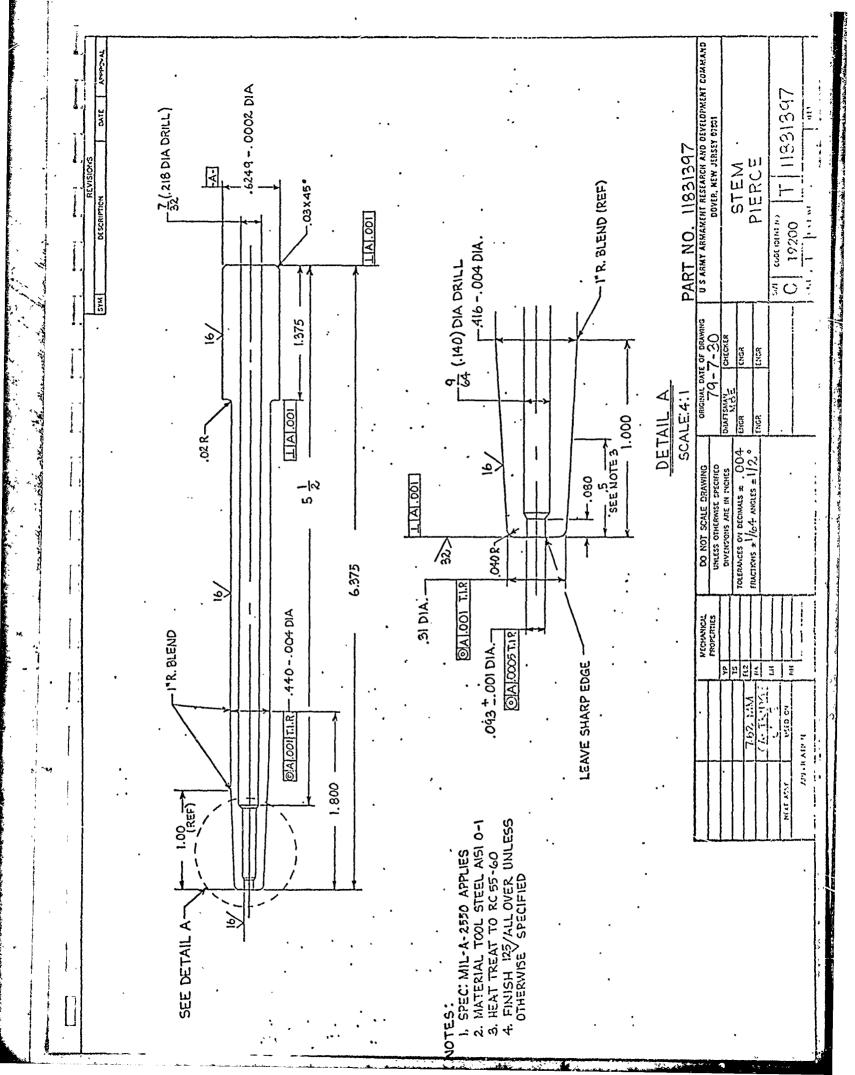
PART NO. 11831395
U S ARMY ARKAMENT RESEARCH AND DEVELOPMENT COMMAND DOVER, NEW JERSEY OFFI 11831395 PUNCH - PIERCE 1-19200 19200 1 C DO NOT SCALE DRAWING
UNLESS OTHERWISE SPECIFICO
DINCHISIONS ARE IN INCHES
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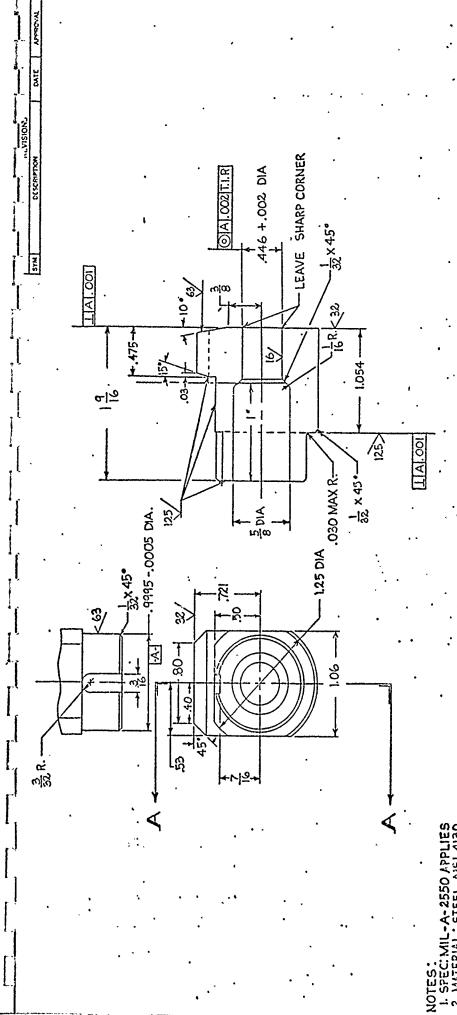


REVISIONS

PART NO. 11831396

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		MECHANICA:	DO NOT SCALE DRAWING	ORICINAL DATE OF DRAWING	U S ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
		PROPERTIES	UNLESS OTHERWISE SPECIFIED	79-7-23	DOVER, NEW JERSEY 07331
		λb	DIVENSIONS ARE IN INCHES	ORAFTS WAY CHECKER	1000
		TS	TOLERANCES ON DECIMALS # . OO4 ENGR	Erich	らしこりだーアしてこ
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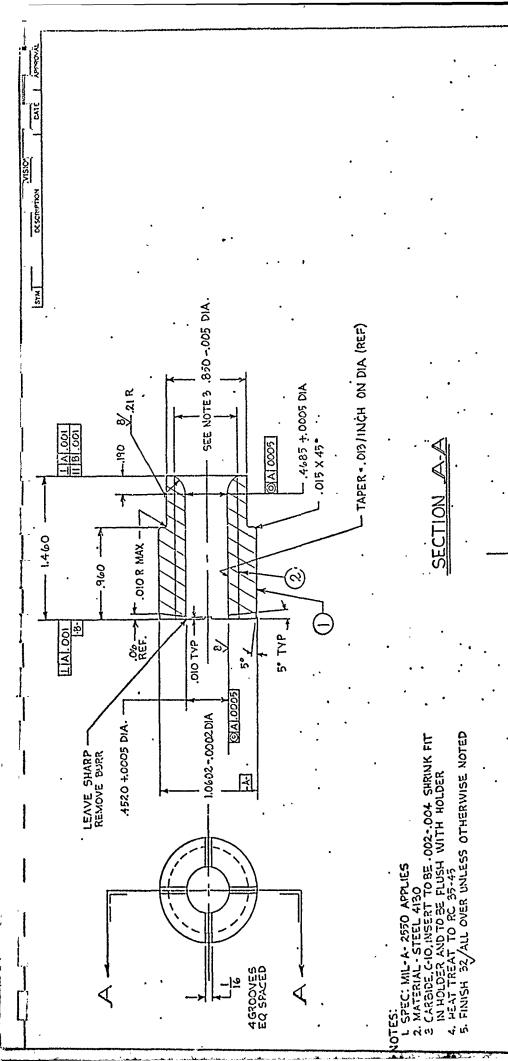




SECTION A-A

	_			_		_	_				
PART NO. 11831398	U S ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND	DOVER, NEW JERSEY 67201		STRIPPER	LCLIC	アードカイド		312 COOL 101 NI W	T 1831393		
	ORIGINAL DATE OF DRAWING	79-7-26	DRAFTS CHECKER	ENGS ENGS		ENGR ENGR			•		
•	DO NOT SCALE DRAWING	· UNLESS OTHERWISE SPECIFIED	DIMENSIONS ARE IN INCHES	TOLERANCES ON DECIMALS # OOG SENCE	0 C/1 - 321000 D7/1 - 3100000	TWIND X 10+ WINES X 1/ Y					
	MECHANICAL	PROPERTIES	٨۶	12	. 25	Y.		100			
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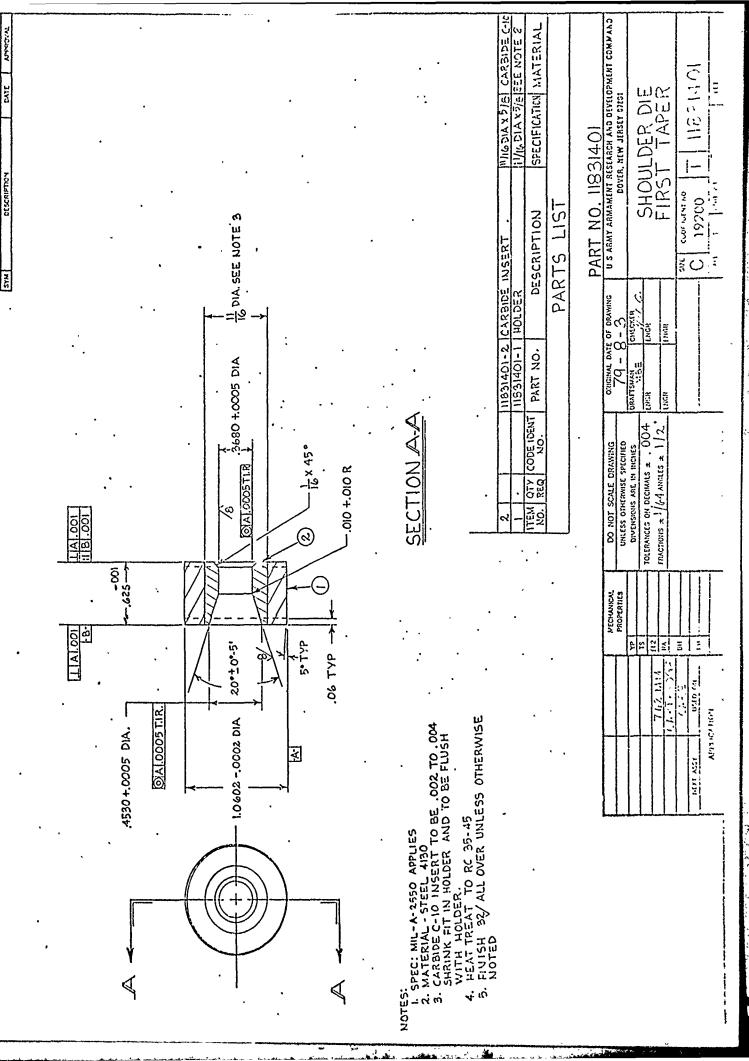
MEXT ASSY

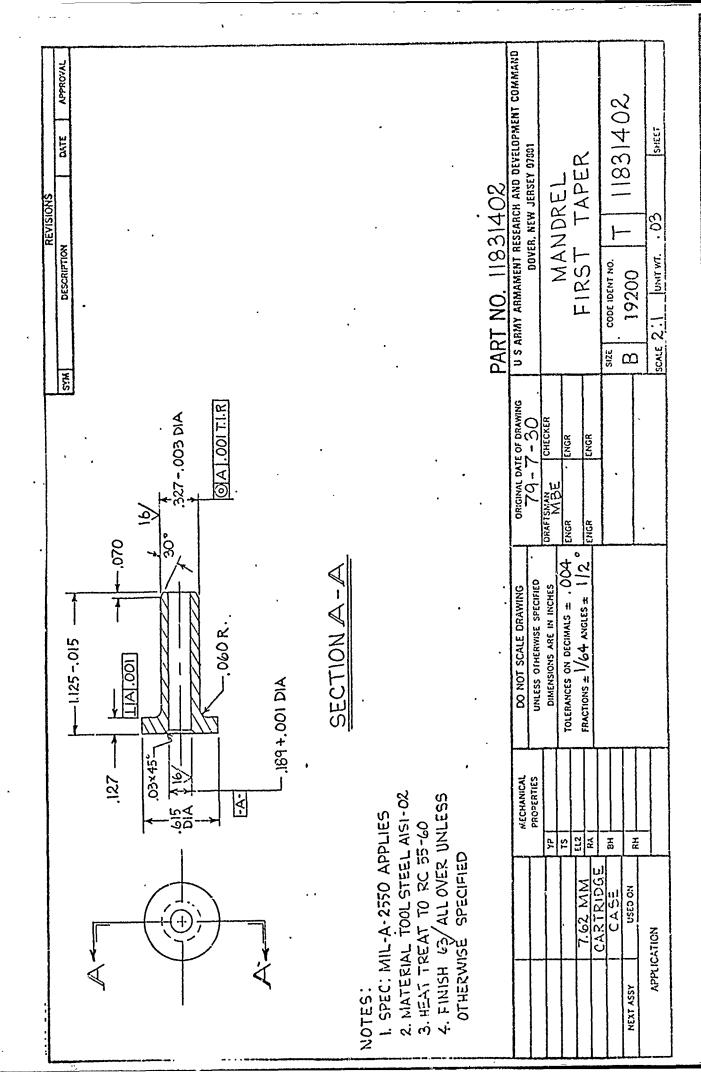


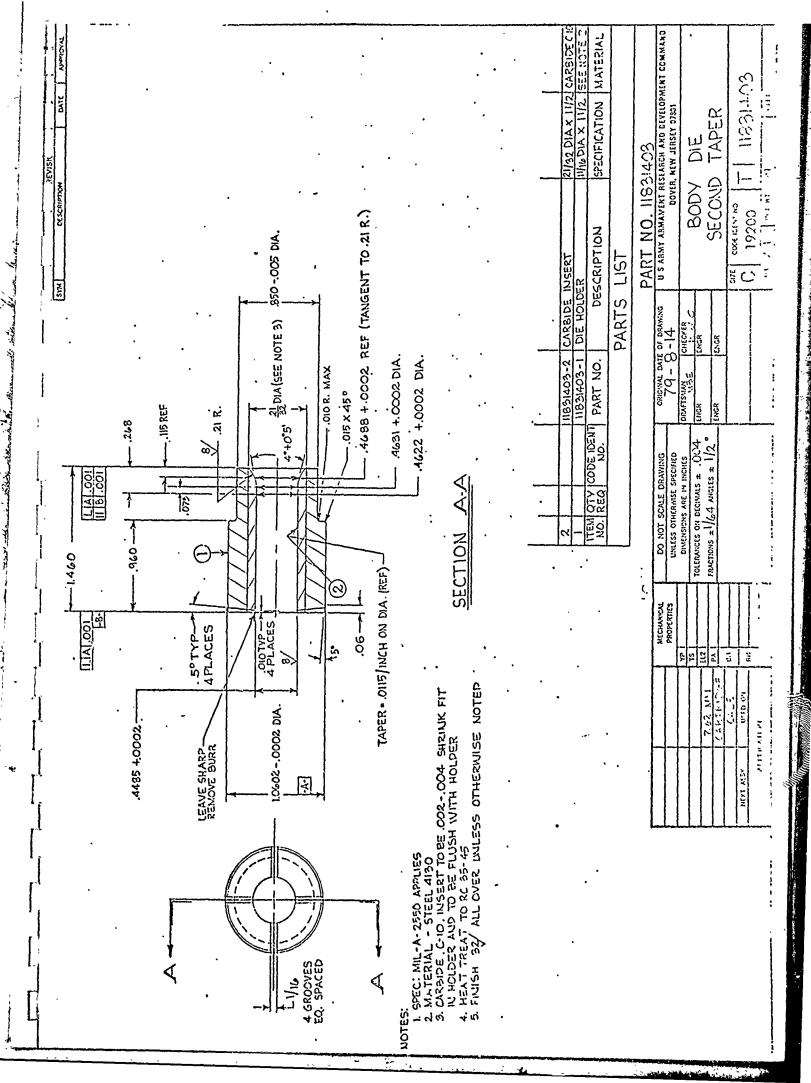
Г		11831400-2	11831400-2 CARBIDE INSERT	2132 514 × 11/2 CARBIDECIO	CARBIDERIO
Γ		11831400-1 HOLDER	HOLDER	11/165:A * 11/2 LG STEEL- 4190	STEEL-4130
>0	CODE IDENT NO.	NO. REG. NO. NO.	DESCRIPTION	SPECIFICATION MATERIAL	MATERIAL
1			PARTS LIST		

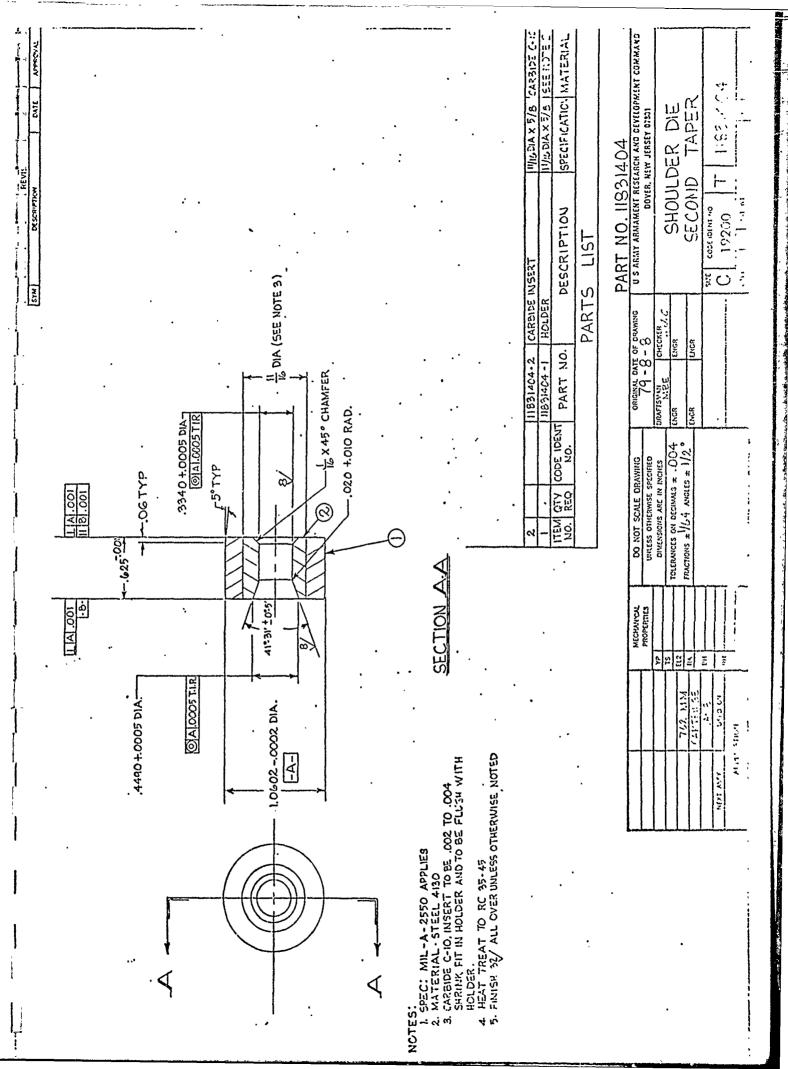
PART NO. 11831400

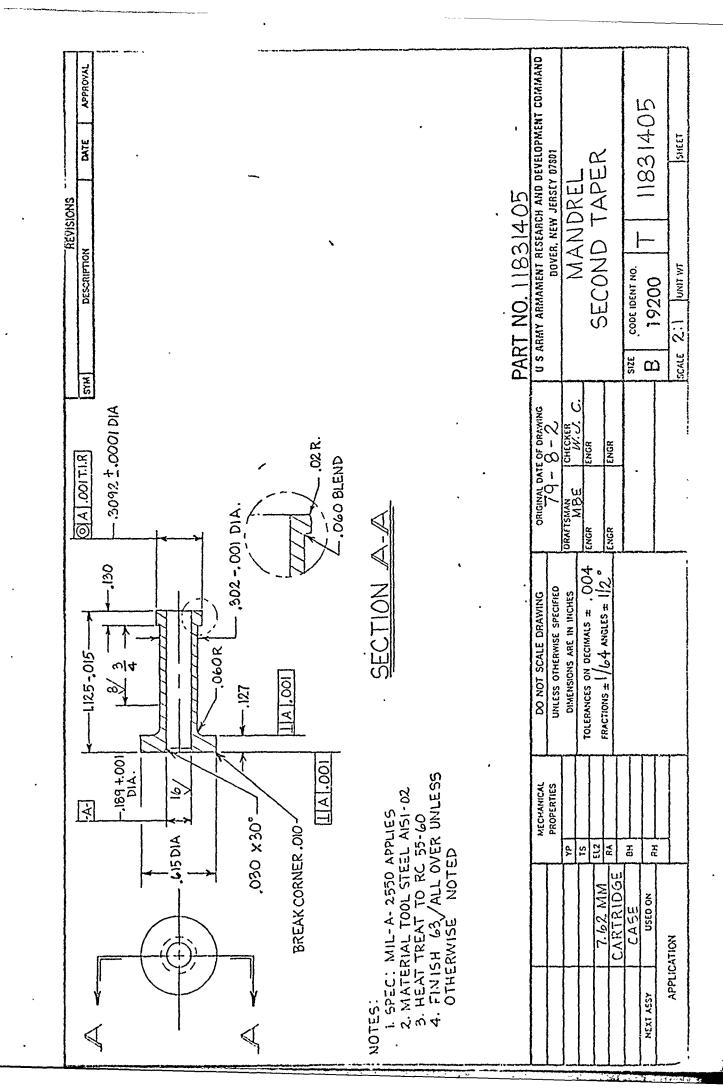
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		d,		DIMENSIONS ARE IN INCHES	DRAFTSWAY CHECKER	ווע /עעמ	
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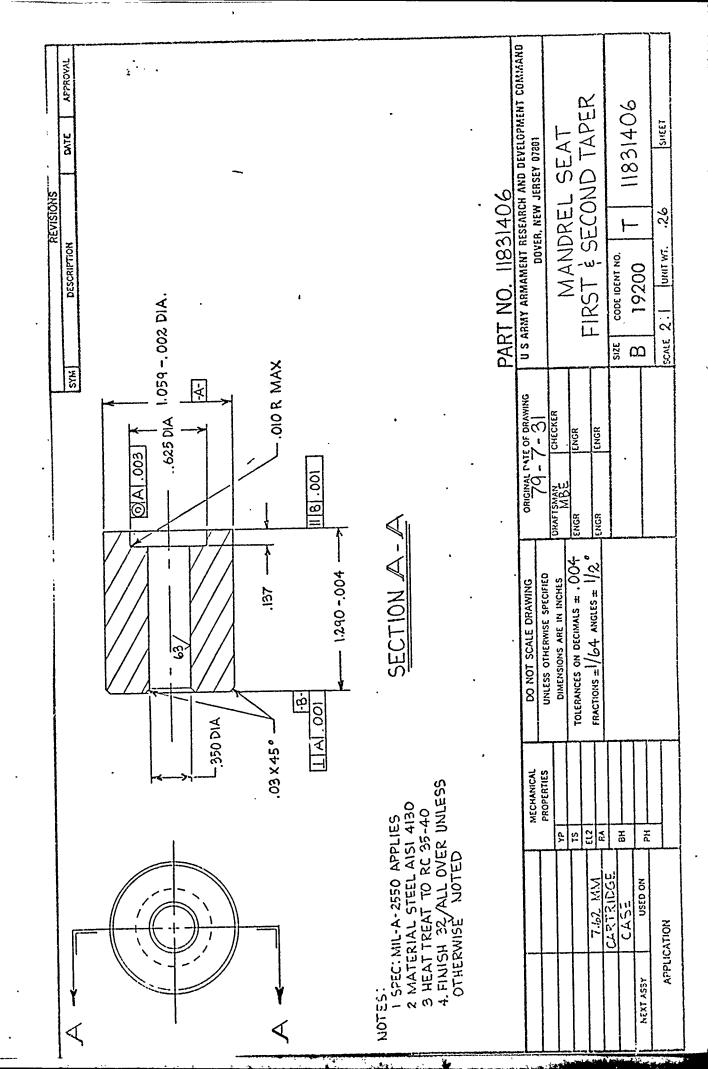


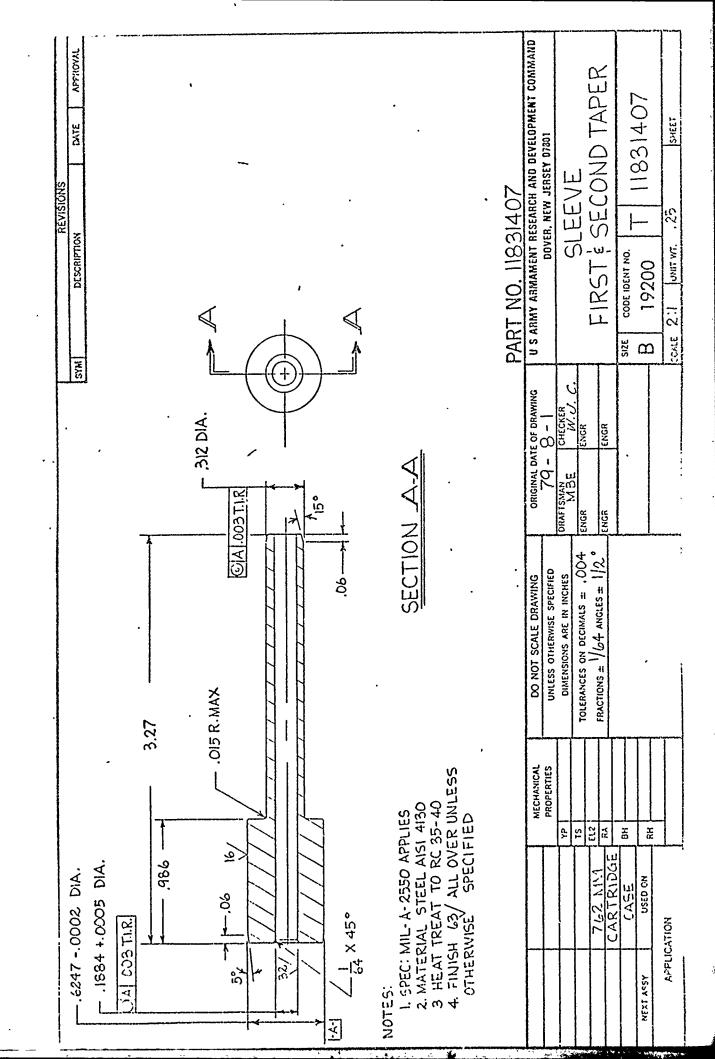












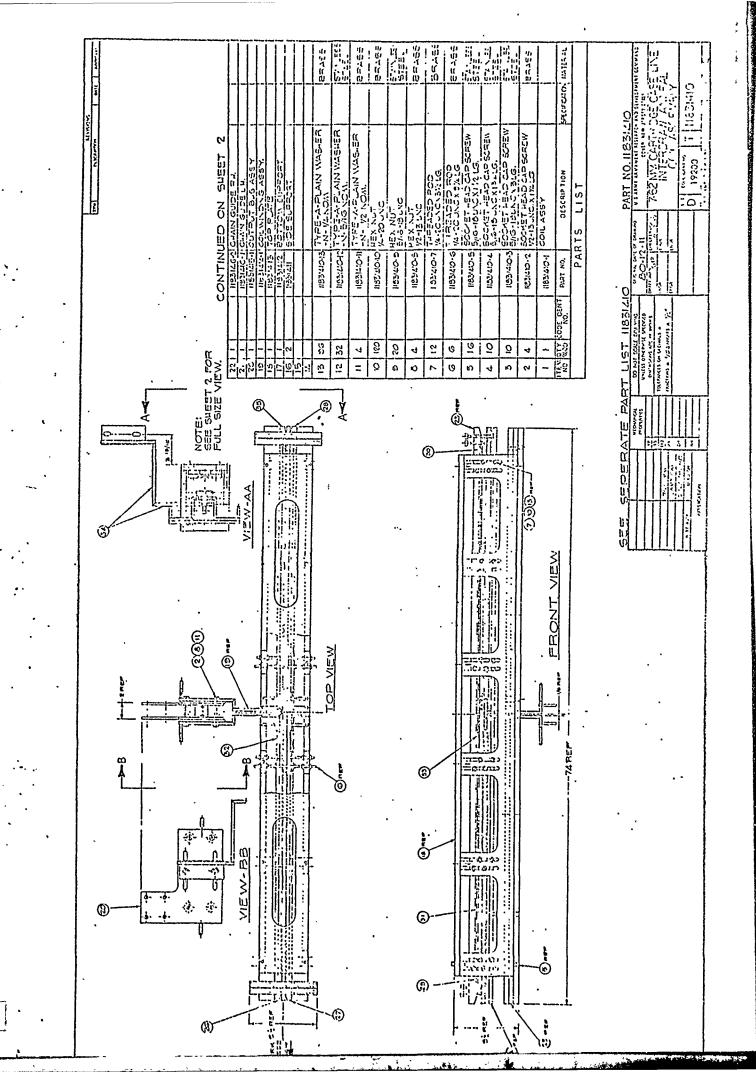
ATTACHMENT 2 COIL DRAWINGS

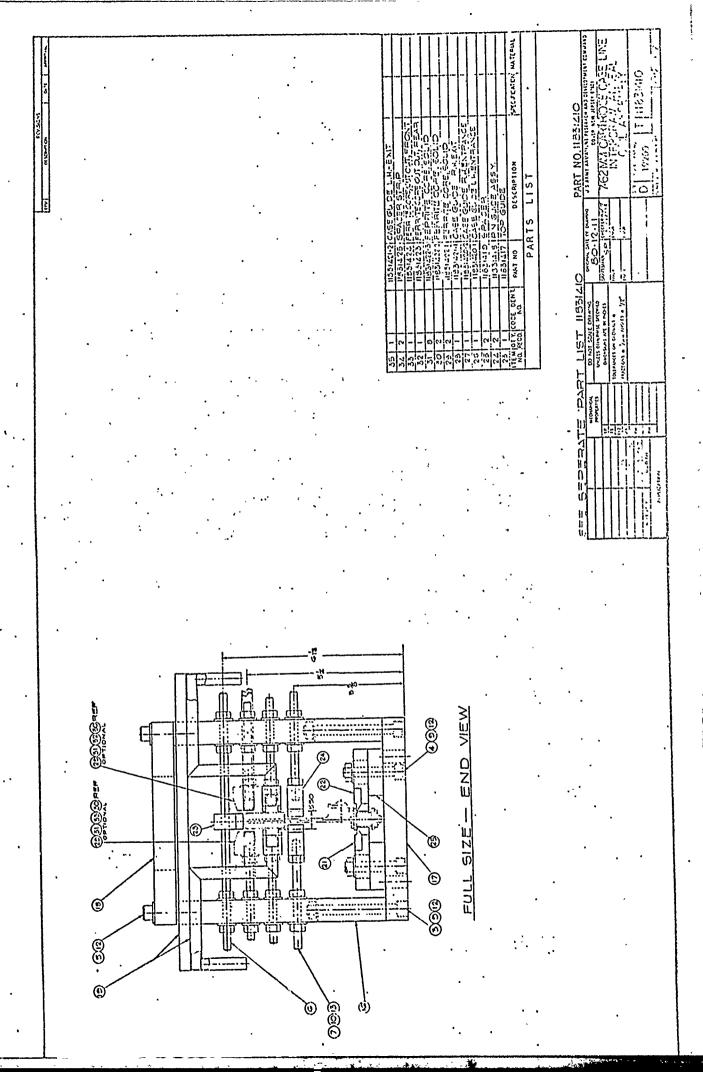
101 Chester Road . Swarthmore, Pennsylvania 19081.

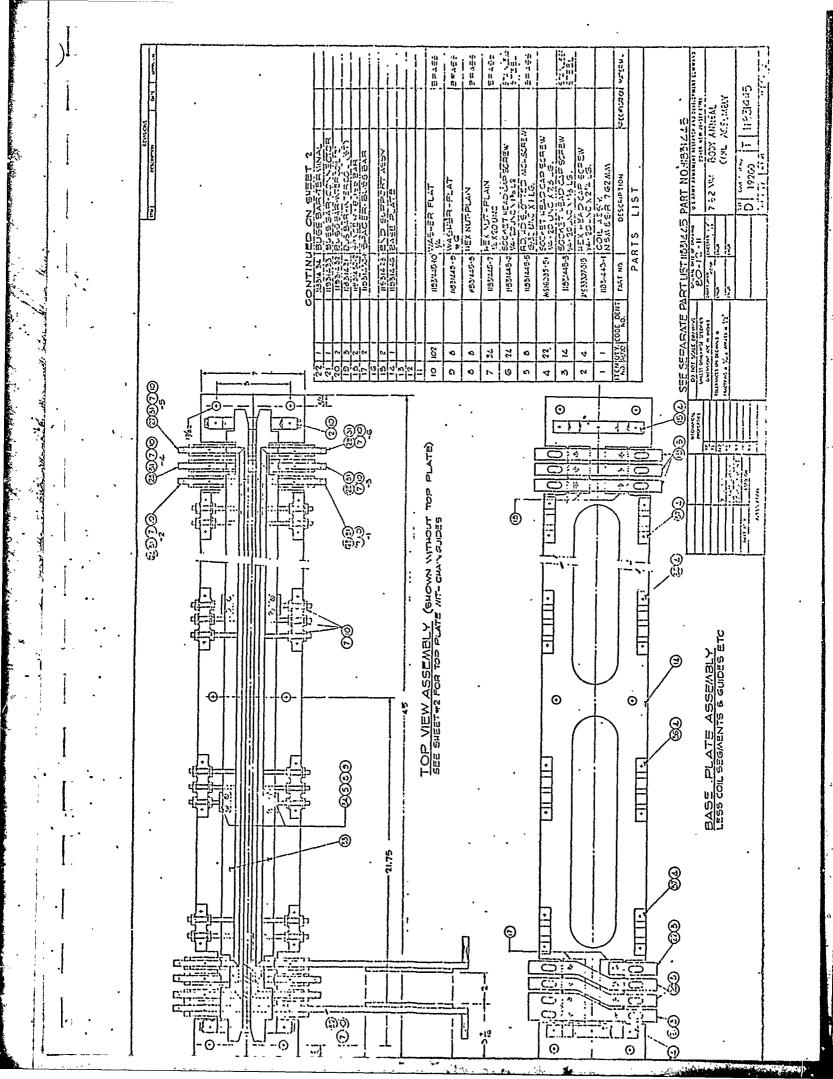
Interdraw Anneal Coil Assembly	11831410
Side Support	11831411
Bottom Support	11831412
Top Plate	11831413
Coil Winding Assembly	11831414
Output Buss Assembly	11831415
Chain Guide	11831416
Top Guide	11831417
Pin Guide Assembly	11831418
Spacer .	11831419
Case Guide, Entrance	11831420
Case Guide, Exit	11831421
Ferrite Core, Solid	11831422
Ferrite Core, Cut Out	11831423
Ferrite Core, Cut Out - Front	11831424
Spacer Strip	11831425
Stress Relief	11831426
Base Plate	11831427
End Support Assembly	11831428
Bracket Assembly	11831429
Spacer - Buss Bar	11831430
Buss Bar - Intercoil	11831431
Buss Bar - Intercoil	11831432
Buss Bar - Connector	11831433
Buss Bar - Terminal	11831434
Neck & Mouth Anneal - Coil Assembly	11831435
Spacer, Coil	11831436
Coil Connector	11831437
Case Guide	11831438
Support Assembly, Case Guide	11831439
Clip Guide Assembly	11831440
Case Pressure Bar Assembly	11831441
Side Support Assembly	11831442

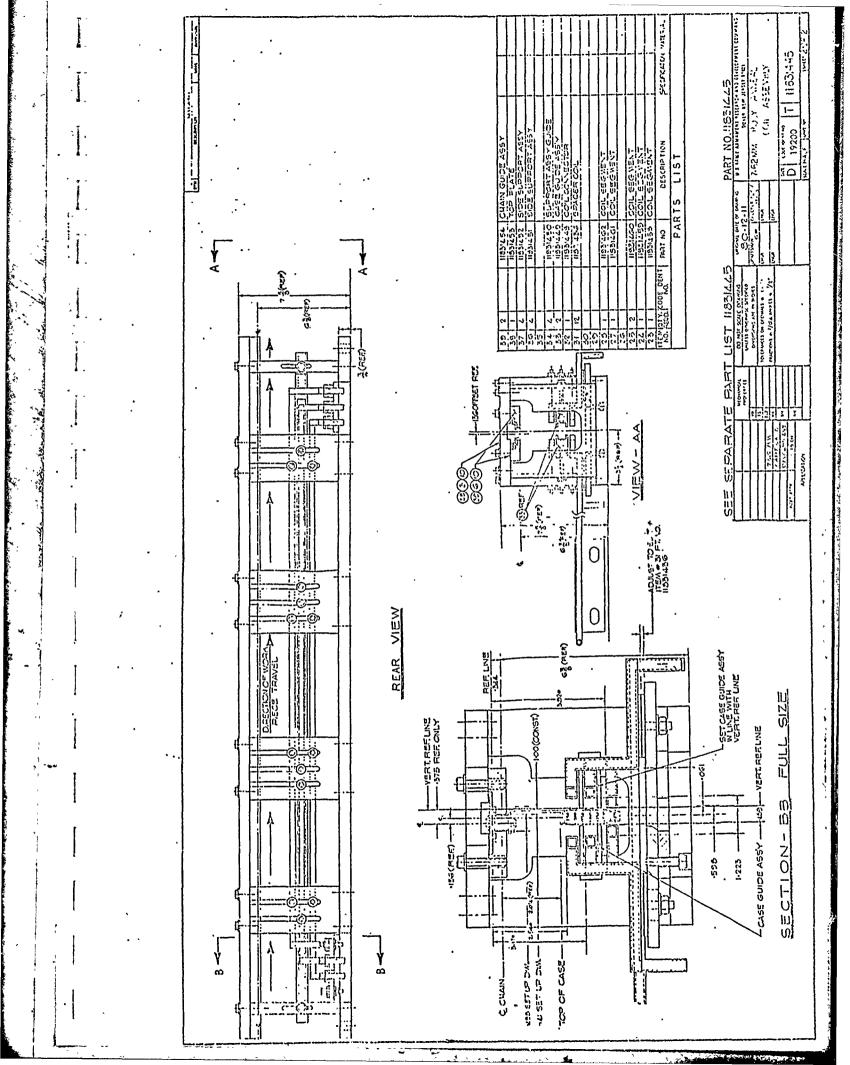
101 Choster Road • Swarthmore, Pennsylvania 19081

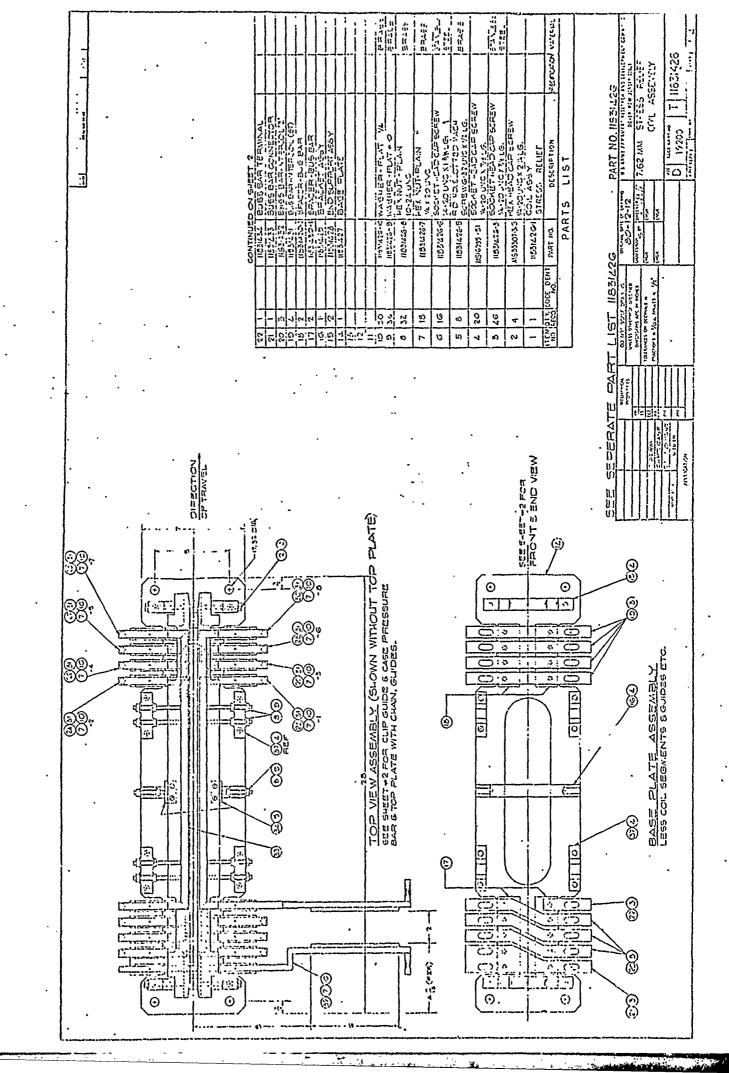
Top Plate .	11831443
Chain Guide Assembly	11831444
Body Anneal Coil Assembly	11831445
Base Plate	11831446
Coil Segment	11831447
Coil Connector	11831448
Case Guide Assembly	11831449
Support Assembly, Case Guide	11831450
Side Support Assembly	11831451
Side Support Assembly	11831452
Top Plate	11831453
Chain Guide Assembly	11831454
Laminated Magnetic Flux Concentrator	11831456
Coil Segment	11831458
Coil Segment	11831459
Coil Segment	11831460
Coil Segment	11831461
Coil Segment	11831462
Coil Segment	11831463
Coil Segment	11831464
Coil Segment	11831465
Coil Segment	11831466
Coil Segment	11831467
Coil Segment	11831468
Coil Segment	11831469
Coil Segment	11831470

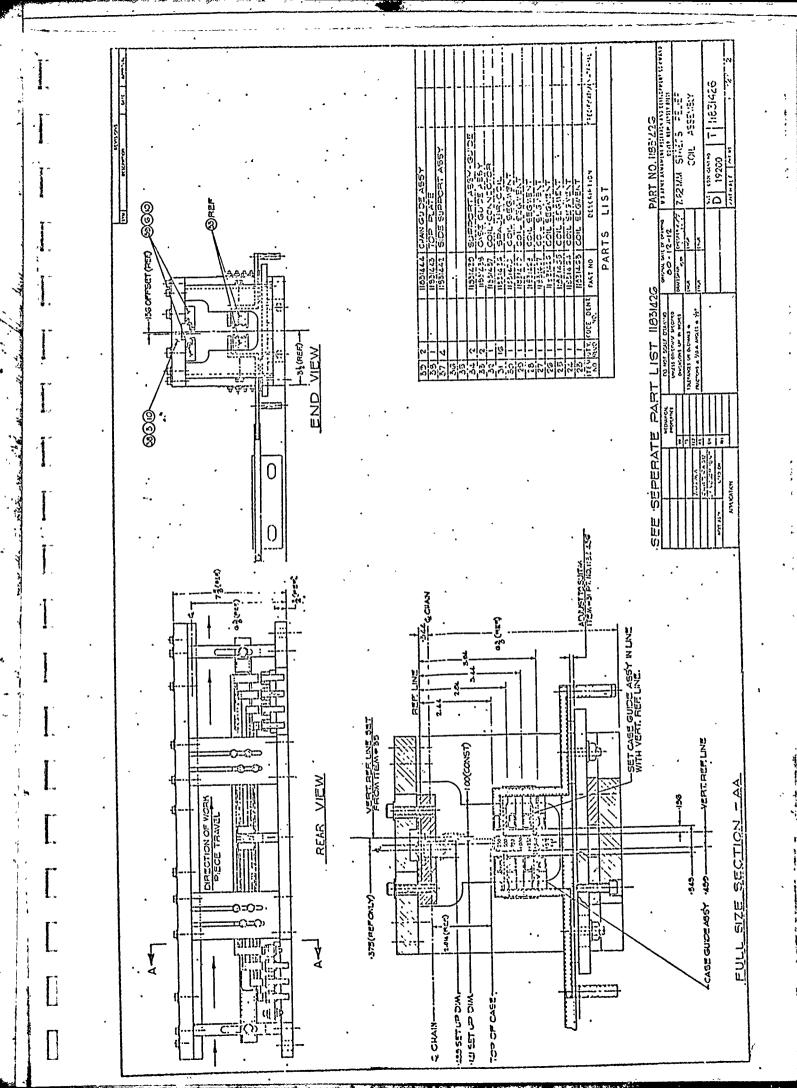


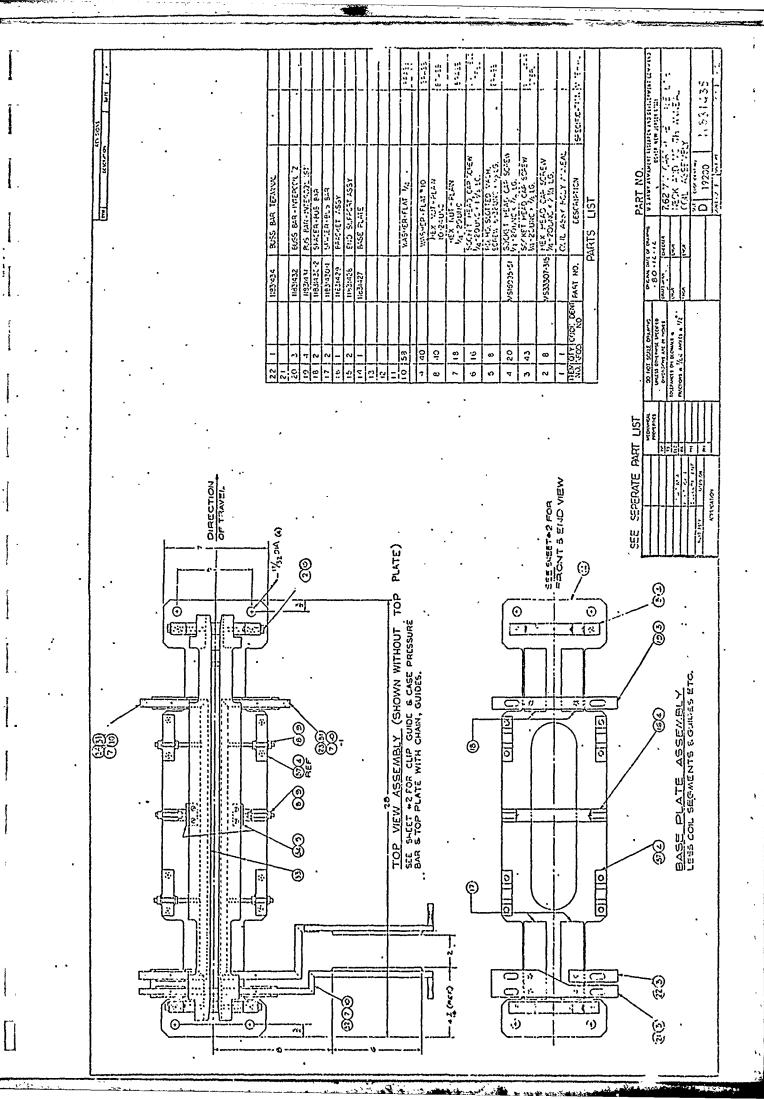


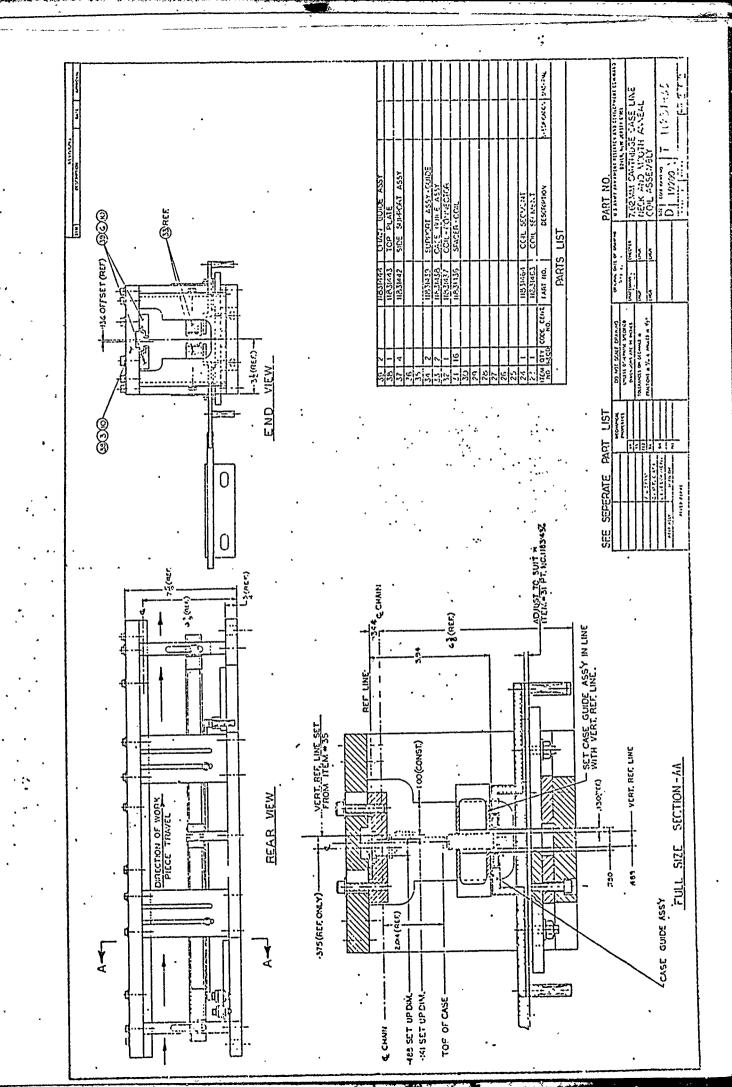








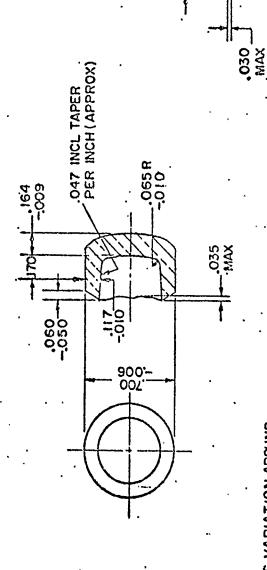




101 Chester Road • Swarthmore, Pennsylvania 19081

ATTACHMENT 3 IN-PROCESS PART DEFINITIONS

2-8-67 22 (1) SEE EO#S 90016 191095#03 gra Ø



NOTES:-

-WALL THICKNESS VARIATION AROUND THE PERIPHERY AT ANY SPECIFIED POINT ALONG THE CYLINDRICAL LENGTH OF THE CUP SHALL NOT VARY MORE THAN .005 - COPPER ALLOY NO. 260, ANNEALED, SPEC MIL-C-50 CUP SPEC MIL-C-10375(MU)

PART NO. 10522459

PERMISSIBLE

19200 CODE IDENT NO.

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<u> </u>	<u>Q</u>	PROPERTIES	N INCHES	Or DRAWING APRIL 13, 1962 iv. NA	i. 75	ADEL .
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Advanced Development and Engineering Center

101 Chester Road • Swarthmore, Pennsylvania 19081

Overall Length	1.19 1.55 2.075
Base Thickness	.170/.174 .170/.174 .176/.180
Wall Thickness (Distance from Inside Base)	.030/.032 (.875) .021/.023 (.875) .032/.036 (.280) .011/.014 (1.700)
Outside Diameter	.539/.542 .525/.527 .468/.469
<u>DRAM</u>	First Draw Second Draw Third Draw

Flat Diameter	.46 minimum
Web Thickness	.072/.078

Web Thickness .036/.040

PRE-POCKET

Web Thickness	.072/.078

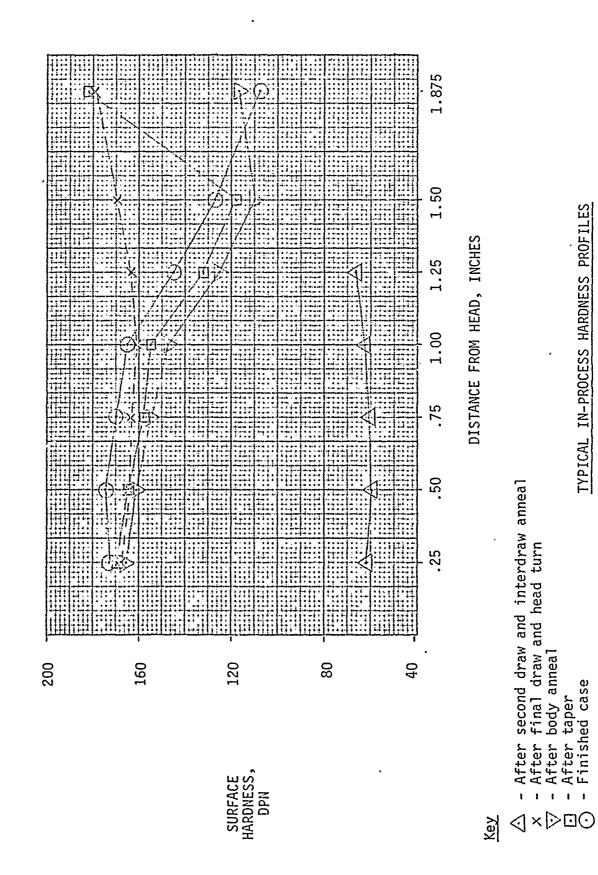
Head-to-Shoulder Length

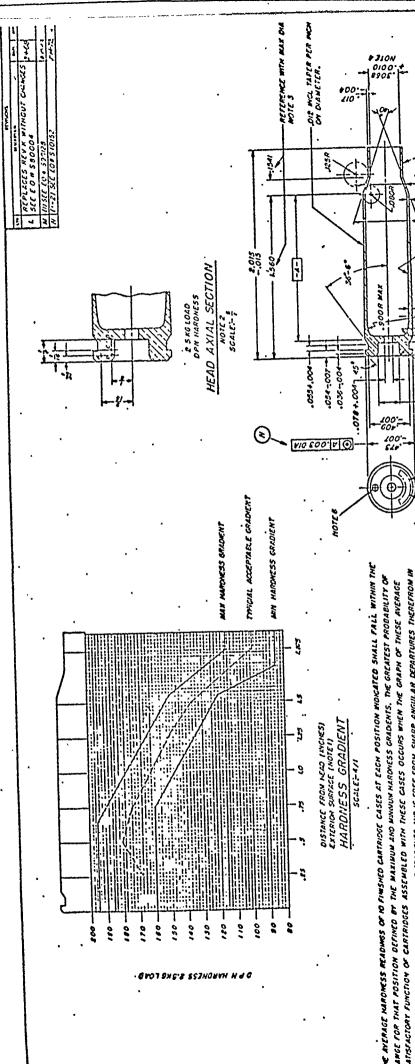
FIRST TAPER

IN-PROCESS PART DEFINITIONS

TYPICAL IN-PROCESS HARDNESS PROFILES

101 Choster Road • Swarthmore, Ponnsylvania 19081





CADINGS IS CENERILLY PARALLEL TO THE LIMIT COLDENTS AND IS FREE FROM SHARP ANGULAN DEPARTURES THEREFROM IN that position defined by the maxibum and winnum haroness gradents. The greatest prodability of INSTACTORY FUNCTION OF CARTRIDGES ASSEMBLED WITH THESE CASES OCCURS WHEN THE GRAPH OF THESE AVERAGE R AEGICH OS FROM THE MERD TO 1.813" FROM THE MEAD.

VINCUM MARONESS AT POINT A TO BE 163 OP M. MINIMUM HARDHESS AT POINTS B, CAND D TO BE 180 OP IL MARONESS

000 NIN SIO

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.126 +.005 .059 KIN.

NOTES 789

201 BASIC

ALL BE DETERWINED ON SECTIONED CASE.

WENSIONS GIVEN AT MITRISECTION OF LINES.

MENSIONS AT PLUGGING OPERATION FOLLOWING TAPER (INFORMATIONAL).

I INCLUSEO TAPER POT TO EXCEED, GOP IS ALLOWABLE OF NECK OUE TO VARIABLE EXPANSION OF BRASS.

KTO IDENTIFICATION WARK.

IMP INITIALS OF MANUFACTURER OR RECOGNIZED TRADE MARK.

TAMP LAST THO FIGURES OF YEAR OF MANUFACTURE.

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SOOR MAK ARE CONSTRUCTION DINCHSIONS WHICH INSURE

ATERIAL: COPPER ALLOY NO. 250, ANNEALED, SPEC MI-C-50

UP (3 DATA), DAT & 10527459, ADVISORY

		CASE	,		100701	
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The bear		2	1		<u>.</u>	_

PART Na. 1052199,7



Advanced Development and Engineering Center

DIMENSIONAL INSPECTION DATA ATTACHMENT 4

01 Chester Road • Swarthmore, Pennsylvania 19081

PARAMETER	DWG. 10521997 TOLERANCE	 1	2	ო	4.	വ	9	AVERAGE	
Web Thickness	.059 min.	920.	9/0.	.078	.077	.077	.074	.076	
Pocket Depth	.126 + .005	.130	.130	.130	.130	.130	.130	.130	
Pocket Diameter .	.2093 + .005	.2093	.2093	.2093	.2093	.2093	.2093	.2093	
Groove Diameter	.409007	.405	.407	.406	.406	.406	.406	.406	
Head Diameter	.473007	.468	.468	.469	.468	.469	.468	.468	
Head Thickness	.054007	.051	.051	.050	.052	.051	.051	.051	
Wall Thickness (.250)	.0305 min.	.034	$\frac{.033}{.036}$.034	$\frac{.034}{.036}$.034	.033	.034	
Mouth Wall Thickness	.017004	.015	$\frac{.016}{.016}$	$\frac{.014}{.016}$	$\frac{.015}{.016}$	$\frac{.015}{.016}$	$\frac{.015}{.016}$	$\frac{.015}{.016}$	
Mouth Diameter	.3067 + .001	.3070	.3075	.3075	.3070	.3070	3075	.3073	
Length to Shoulder	1.634006	1.631	1.632	1.632	1.632	1.631	1.631	1.6315	
Overall Length	2.015015	2.007	2.006	2.007	2.008	2.006	2.008	2.007	
Min./Max. Profile			Ö						

DIMENSIONAL INSPECTION DATA

No. 30012

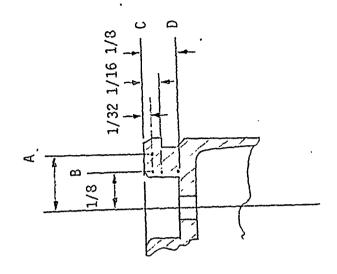


Advanced Development and Engineering Center

101 Choster Road • Swarthmore, Pennsylvania 19081

ATTACHMENT 5 METALLURGICAL INSPECTION DATA

101 Chester Road • Swarthmore, Pennsylvania 19081

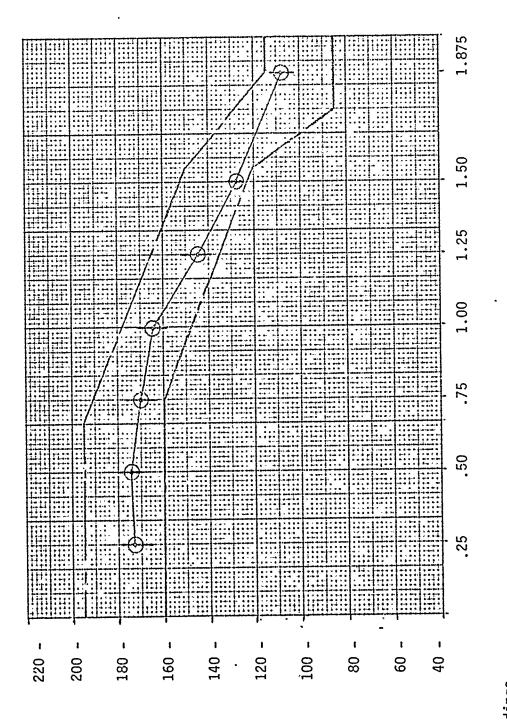


INTERNAL HEAD HARDNESS

AVERAGE DPN 169.0 198.0 199.0

A B C C

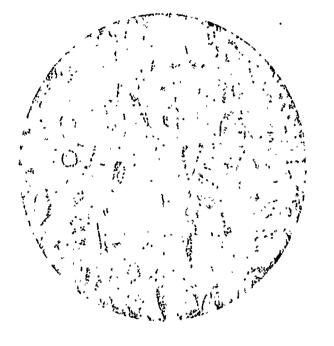
101 Chester Road . Swarthmore, Pennsylvania 19081



DISTANCE FROM HEAD, INCHES

FINAL CASE HARDNESS GRADIENT

Key
Range of readings
Average
Specified limits



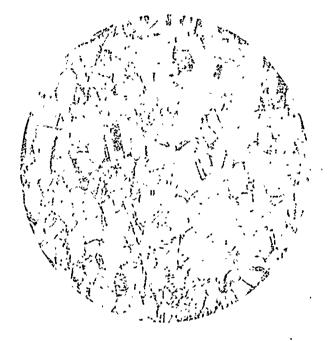
500 from head

.250 from head

magnification 75x

GRAIN STRUCTURE MICROPHOTOGRAPHS

01 Chester Road . Swarthmore, Pennsylvania 19081



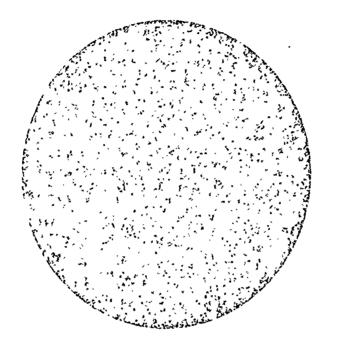
000 from head

.750 from head

Magnification 75x

GRAIN STRUCTURE MICROPHOGRAPHS

101 Chester Road • Swarthmore, Pennsylvania 19081



1.500 from head

Magnification - 75x

1.250 from head

GRAIN STRUCTURE MICROPHOGRAPHS

Advanced Development and Engineering Center

101 Chester Road • Swarthmore, Pennsylvania 19081

ATTACHMENT 6 TEST FIRING DATA

H. P. WHITE LABORATORY, INC.

3114 Scarboro Road • Street, Maryland 21154 (301) 838-6550

RECEIVED

NOV 3 1980

K. H.



30 October 1980 (HPWLI 2483)

Gulf and Western Industries, Inc. 101 Chester Road Swarthmore, Pennsylvania 19081

Attention: Mr. K. Hall

Gentlemen:

In accordance with your Purchase Order No. 78625-02, H.P. White Laboratory, Inc. conducted firing tests of twenty (20) experimental 7.62mm brass cartridge cases.

A propellent loading was developed which would produce the pressures specified for the caliber 7.62mm, M80 High Pressure Test (proof) cartridge. The cases were primed and loaded in accordance with that loading and the cartridges fired in a pressure barrel configured to determine peak chamber pressures in copper units of pressure (CUP). Table I is a summary of the attached data record of these firings.

TABLE I. SUMMARY OF RESULTS

Propellent Load (1)			re (CUF x		
(grains)	Number Fired	Maximum	Minimum	Average	(2)
41.0 to 44.0 (3)	7	62.2	56.5	59.7	
41.5 to 42.0 (4)	2	62.2	61.3	61.8	
42.5 (4)	11	69.0	64.4	66.3	
 (1) IMR 4475 propellent (2) MIL-Spec average pres (3) 150 grain bullet. (4) 180 grain bullet. 	ssure for M80:	67,500 + 25	500 PSI.		

Gulf and Western Industries, Inc. Attention: Mr. K. Hall 30 October 1980 Page 2

Subsequent to these tests the spent cases were examined for evidence of cracks, bulging, distortion, primer leakage, etc. No deficiencies were noted.

The spent cases are being returned via United Parcel Service under separate cover. Should you have any questions regarding this matter or if we may be of any further service, please do not hesitate to contact us.

Very truly yours,

H.P. WHITE LABORATORY, INC.

D.R. Dunn

DRD/1t enclosures

Ammunition: 7.62 handloads	83
Primer: CCI 100	
Powder: gr. IMR 4475 On: Seating Depth:	
Pullet	
No. Pressure Darret Ser. No.: Bbl. Length: Twist: Twis	
Required VELOCITY films f. p. s. Lo 4,00 Lo 41.0 Lo 150 gr. FMC	
Boce	
No.	
No. Cver 20 fr. 6 15 Le p. s. i. Bullet 1	
No. Cver 20 fr. 6 15 Le p. s. i. Bullet 1	
1	
2	
3	
4 .007096 2818.8 .518 58700 43.0 5 .006951 2877.6 .309 62600 43.5 6 .007022 2848.5 .311 61700 43.7 7 .006973 2868.6 .310 62200 44.0 8 .007631 2621.2 .312 61300 41.5 180 gr. SP 9 .007567 2643.0 .310 62200 42.0 10 .007458 2681.6 .298 67600 42.5 11 .007472 2677.0 .304 64800 42.5 12 .007495 2668.8 .295 69000 42.5 13 .007496 2668.4 .303 65300 42.5 14 .007512 2662.7 .305 64400 42.5 15 .007477 2675.2 .300 66700 42.5 16 .007512 2662.7 .304 64800 42.5 17 .007500 2666.6 .301 66200 42.5 18 .007472 2677.0 .296 68600 42.5 19 .007498 2667.7 .299 67200 42.5 19 .007498 2667.7 .299 67200 42.5 19 .007520 2659.5 .305 64400 42.5 20 .007520 2659.5 .305 64400 42.5 20 .007520 2659.5 .305 64400 42.5 30 .007520 2659.5 .305 64400 42.5 42 .007520 2659.5 .305 64400 42.5 17 .007500 2666.6 .301 .301 .301 .301 18 .007472 .2077.0 .296 .3040 .42.5 20 .007520 .305 .305 .305 .305 .305 .305 30 .307 .307 .307 .307 .307 30 .307 .307 .307 .307 .307 .307 30 .307 .307 .307 .307 .307 .307 .307 30 .307 .	
5 .006951 2877.6 .309 62600 43.5 6 .007022 2848.5 .311 61700 43.7 7 .006973 2868.6 .310 62200 44.0 8 .007631 2621.2 .312 61300 41.5 180 gr. SP 9 .007567 2643.0 .310 62200 42.0 10 .007488 2681.6 .298 67600 42.5 11 .007472 2677.0 .304 64800 42.5 12 .007495 2668.8 .295 69000 42.5 13 .007496 2668.8 .295 69000 42.5 14 .007512 2662.7 .305 64400 42.5 15 .007477 2675.2 .300 66700 42.5 17 .007500 2666.6 .301 66200 42.5 18 .00742e 2677.0 .296 68600 42.5 <t< td=""><td></td></t<>	
6 .007022 2848.5 .311 61700 43.7 7 .006973 2868.6 .310 62200 44.0 8 .007631 2621.2 .312 61300 41.5 180 gr. SP 9 .007567 2643.0 .310 62200 42.0 10 .007458 2681.6 .298 67600 42.5 .11 .007472 2677.0 .304 64800 42.5 .12 .007495 2668.8 .295 69000 42.5 .13 .007496 2668.4 .303 65300 42.5 .14 .007512 2662.7 .305 64400 42.5 .15 .007477 2675.2 .300 66700 42.5 .16 .007512 2662.7 .304 64800 42.5 .17 .007500 2666.6 .301 66200 42.5 .18 .007472 2677.0 .296 68600 42.5 .19 .007498 2667.7 .299 67200 42.5 .20 .007520 2659.5 .305 64400 42.5	
Residence Section Se	
8 .007631 2621.2 .312 61300 41.5 180 gr. SP 9 .007567 2643.0 .310 62200 42.0 10 .007458 2681.6 .298 67600 42.5 11 .007472 2677.0 .304 64800 42.5 12 .007495 2668.8 .295 69000 42.5 13 .007496 2668.4 .303 65300 42.5 14 .007512 2662.7 .305 64400 42.5 15 .007477 2675.2 .300 66700 42.5 16 .007512 2662.7 .304 64800 42.5 17 .007500 2666.6 .301 66200 42.5 18 .007472 2677.0 .296 68600 42.5 19 .007498 2667.7 .299 67200 42.5 20 .007520 2659.5 .305 64400 42.5 Velocity Pressure CLIENT Average: Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Date: 30 October 1980	
9 .007567 2643.0 .310 62200 42.0 10 .007458 2681.6 .298 67600 42.5 .11 .007472 2677.0 .304 64800 42.5 .12 .007495 2668.8 .295 69000 42.5 .13 .007496 2668.4 .303 65300 42.5 .14 .007512 2662.7 .305 64400 42.5 .15 .007477 2675.2 .300 66700 42.5 .16 .007512 2662.7 .304 64800 42.5 .17 .007500 2666.6 .301 66200 42.5 .18 .007472 2677.0 .296 68600 42.5 .19 .007498 2667.7 .299 67200 42.5 .20 .007520 2659.5 .305 64400 42.5	
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Velocity Pressure Velocity Pressure Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Date: 30 October 1980	
Velocity Pressure CLIENT Average: Extreme Var.: Standard Dev. Range Conditions: Barometer: US MIL Spec. Average pressure: 67,50 CLIENT Gulf and Western Date: 30 October 1980	
Velocity Pressure CLIENT Average: Extreme Var.: Standard Dev. Range Conditions: Barometer: US MIL Spec. Average pressure: 67,50 CLIENT Gulf and Western Date: 30 October 1980	
Velocity Pressure CLIENT Average: Extreme Var.: Mean Var.: Standard Dev. Range Conditions: Barometer: Date: 30 October 1980	
Average: Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Date: 30 October 1980	500 - 2500
Average: Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Gulf and Western Date: 30 October 1980	
Average: Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Gulf and Western Date: 30 October 1980	
Average: Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Gulf and Western Date: 30 October 1980	
Average: Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Gulf and Western Date: 30 October 1980	
Average: Extreme Var.: Mean Var. Standard Dev. Range Conditions: Barometer: Gulf and Western Date: 30 October 1980	
Mean Var. Standard Dev. Range Conditions: Barometer Date: 30 October 1980	
Standard Dev.	
Range Conditions: Barometer Date: 30 October 1980	
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TIRIVVI	
Wet Bulb Temp.: Chronograph No. Gunner: Mitchem	

Form 21

Advanced Development and Engineering Center

No. 30012

101 Chester Road • Swarthmore, Pennsylvania 19081

ATTACHMENT 7 VOID TEST DATA

Conditions	All 24 stations	· 4 even voids	4 consecutive voids	6 even voids	6 consecutive voids
1-1/2 in.	131.5	128.6	127.9	130.2	123.7
1/2 in.	173.3	170.5	144.7	170.7	130.8
(KW)	104	102	102	101	101
Test	A	മ	, ن	O	ш